

victoria interval

MTOB[pennsylvania]

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april 3, 2013

MTOB final report



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appendix A: cellular beams

A.1 plastic moments

PLASTIC MOMENTS $1/5$

TOP TEE SECTION (W18x35)

$$A_f = b_f t_f = (6)(0.425) = 2.55 \text{ in}^2$$

$$A_w = h_w t_w = (3.575)(0.3) = 1.0725 \text{ in}^2$$

AREA FLANGE BELOW PNA:

$$\frac{1}{2}(A_f - A_w) = \frac{1}{2}(2.55 - 1.0725) = 0.73875 \text{ in}^2 = 0.74 \text{ in}^2$$

DIST TO PNA

$$\frac{A_{\text{below}}}{b_f} = \frac{0.74}{6} = 0.123 \text{ ''}$$

MOMENTS ABOUT PNA

- FLANGE ABOVE

$$A = 2.55 - 0.74 = 1.81 \quad \text{ARM} = \frac{1}{2}(0.425 - 0.123) = 0.151$$
- FLANGE BELOW

$$A = \cancel{0.74} \quad \text{ARM} = \frac{1}{2}(0.123) = 0.0615$$
- WEB

$$A = 1.0725 \quad \text{ARM} = \frac{1}{2}(3.575) = 1.7875$$

$$Z_p = \underbrace{(1.81)(0.151)}_{\text{FL. ABOVE}} + \underbrace{0.74(0.0615)}_{\text{FL. BELOW}} + \underbrace{(1.0725)(1.7875)}_{\text{WEB}} = 2.65 \text{ in}^3$$

$$\sigma = 50 \text{ ksi}$$

$$M_p = (50 \text{ ksi})(2.65 \text{ in}^3) = 132 \text{ k-in}$$

PLASTIC MOMENTS 2/5

MIDDLE WEB, W18x35 (TOP HALF)

$$t_w = 0.30 \text{ in}$$

$$M_p = \frac{bh^2}{4} F_y \quad (\text{RECTANGULAR SECTION})$$

$$= \frac{(0.3)(5.28)^2}{4} F_y \quad \left. \begin{array}{l} \\ \end{array} \right\} 50 \text{ KSI}$$

$$= (2.09 \text{ in}^3)(50 \text{ KSI})$$

$$= \boxed{104.5 \text{ K}\cdot\text{in}}$$

MIDDLE WEB, W18x40 (BOTTOM HALF)

$$t_w = 0.36 \text{ in}$$

$$M_p = \frac{(0.36)(5.28)^2}{4} (50 \text{ KSI})$$

$$= (2.5 \text{ in}^3)(50 \text{ KSI})$$

$$= \boxed{125.5 \text{ K}\cdot\text{in}}$$

PLASTIC MOMENTS 3/5

BOTTOM TEE

$$A_f = b_f t_f = (6.06)(0.605) = 3.6663$$

$$A_w = t_w h_w = (0.36)(3.395) = 1.222$$

AREA FL. BELOW PNA =

$$\frac{1}{2}(A_f - A_w) = \frac{1}{2}(3.6663 - 1.222) = 1.222$$

DIST TO PNA

$$\frac{A_{\text{BELOW}}}{b_f} = \frac{1.222}{6.06} = 0.202 \text{ in}$$

MOMENTS ABOUT PNA

- FLANGE ABOVE
 $A = 3.6663 - 1.222 = 2.4443$ ARM = $\frac{1}{2}(0.605 - 0.202) = 0.2015$

- FLANGE BELOW
 $A = 1.222$ ARM = $\frac{1}{2}(0.202) = 0.101$

- WEB
 $A = 1.222$ ARM = $\frac{1}{2}(3.395) = 1.6975$

$$Z_p = (2.4443)(0.2015) + (1.222)(0.101) + (1.222)(1.6975)$$

$$= 2.69 \text{ in}^3$$

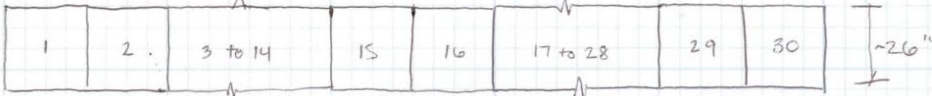
$$\sigma = 50 \text{ KSI}$$

$$M_p = (2.69)(50) = 134.5 \text{ k in}$$

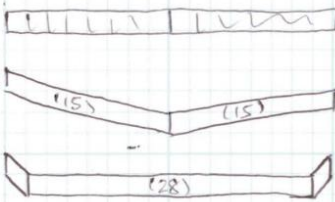
A.2 example plastic analysis calculation

PLASTIC ANALYSIS, UPPERBOUND THM. $\frac{1}{2}$
 EXAMPLE CALCULATION (SEE SPREADSHEET FOR COMPLETE VERSION)

30-CELL CELLULAR BM:

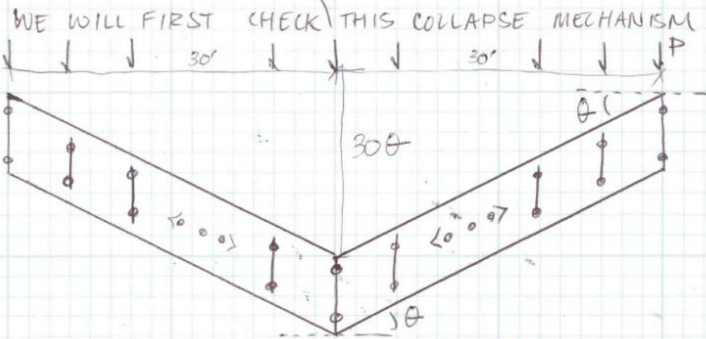


ASSUMING COLLAPSE MECHANISMS WILL ALL BE SYMMETRICAL SINCE THE LOAD IS UNIFORM AND THE SECTIONS ARE SYMMETRICAL
 POSSIBLE MECHANISM SHAPES



AND ALL VARIATIONS B/T THESE TWO

WE WILL FIRST CHECK THIS COLLAPSE MECHANISM:



P IS APPLIED @ EVERY PANEL
 P IS THE COLLAPSE LOAD
 62 TOTAL HINGES

ALSO, NOTE HINGE FORMATION IN THE WEB MEMBERS.
 THIS IS B/C FOR BOTH W18x35, W18x46, WE HAVE:

$$M_{P,WEB} < M_{P,TEE}$$

$$M_{P,WEB, 18 \times 35} = 104.5 \text{ k}\cdot\text{in}$$

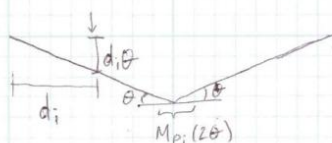
$$M_{P,WEB, 18 \times 46} = 125.5 \text{ k}\cdot\text{in}$$

PLASTIC ANALYSIS, UPPER BOUND THM $\frac{3}{2}$

EX CALCULATION

$$\delta W_{EXT} = \delta W_{INT}$$

$$\sum P_i \delta_i \theta = \sum M_{P_i} \delta_i \theta$$



$$P(2+4+6+\dots+28+30+28+\dots+2)\theta = M_{P_{35}}(2\theta) + 30M_{P_{35}}(\theta) + M_{P_{46}}(2\theta) + 30\theta M_{P_{46}}$$

$$450 P \theta = 32 M_{P_{35}} \theta + 32 M_{P_{46}} \theta$$

$$= 32(104.5) + 32(125.5)$$

$$\Rightarrow P = \frac{7360}{450}$$

$$= 16.3556 \text{ K PER PANEL}$$

$$= \boxed{8.18 \text{ K/FT}}$$

THE EXCEL SPREADSHEET WILL CALCULATE THIS FOR ALL SYMMETRICAL COLLAPSE MECHANISMS TO FIND THE LEAST UPPERBOUND, WHICH WILL BE THE CORRECT MECHANISM

A.3 spreadsheet for (plastic) symmetrical failure mechanisms

| d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | | |
|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|--------------|-----------------------------|-----------------|-----------------------------|-----------------|
| 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | | |
| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | |
| 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | | |
| 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | | |
| 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | | |
| 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | | |
| 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | | |
| 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | | |
| 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | | |
| 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | | |
| 20 | 2 | 20 | 2 | 20 | 2 | 20 | 2 | 20 | 2 | 18 | 2 | 16 | 2 | | |
| 22 | 2 | 22 | 2 | 22 | 2 | 22 | 2 | 22 | 2 | 20 | 2 | 16 | 2 | | |
| 24 | 2 | 24 | 2 | 24 | 2 | 24 | 2 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 26 | 2 | 26 | 2 | 26 | 2 | 24 | 0 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 28 | 2 | 28 | 2 | 26 | 0 | 24 | 0 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 30 | 2 | 28 | 0 | 26 | 0 | 24 | 0 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 28 | 2 | 28 | 2 | 26 | 0 | 24 | 0 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 26 | 2 | 26 | 2 | 26 | 2 | 24 | 0 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 24 | 2 | 24 | 2 | 24 | 2 | 24 | 2 | 22 | 0 | 20 | 2 | 16 | 2 | | |
| 22 | 2 | 22 | 2 | 22 | 2 | 22 | 2 | 22 | 2 | 20 | 2 | 16 | 2 | | |
| 20 | 2 | 20 | 2 | 20 | 2 | 20 | 2 | 20 | 2 | 20 | 2 | 16 | 2 | | |
| 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | 18 | 2 | 16 | 2 | | |
| 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | 16 | 2 | | |
| 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | 14 | 2 | | |
| 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | 12 | 2 | | |
| 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | 10 | 2 | | |
| 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | 8 | 2 | | |
| 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | 6 | 2 | | |
| 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | 4 | 2 | | |
| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | |
| 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 2 | | |
| 62 | | 60 | | 56 | | 52 | | 48 | | 44 | | 40 | | 36 | |
| $\delta_{ext} = P*\theta^*$ | 450 | $\delta_{ext} = P*\theta^*$ | 448 | $\delta_{ext} = P*\theta^*$ | 442 | $\delta_{ext} = P*\theta^*$ | 432 | $\delta_{ext} = P*\theta^*$ | 418 | $\delta_{ext} = P*\theta^*$ | 400 | $\delta_{ext} = P*\theta^*$ | 378 | $\delta_{ext} = P*\theta^*$ | 352 |
| $\delta_{ext} = \theta^*$ | 7360 | $\delta_{ext} = \theta^*$ | 6900 | $\delta_{ext} = \theta^*$ | 6440 | $\delta_{ext} = \theta^*$ | 5980 | $\delta_{ext} = \theta^*$ | 5520 | $\delta_{ext} = \theta^*$ | 5060 | $\delta_{ext} = \theta^*$ | 4600 | $\delta_{ext} = \theta^*$ | 4140 |
| P= | 16.35556 | P= | 15.40179 | P= | 14.57014 | P= | 13.84259 | P= | 13.20574 | P= | 12.65 | P= | 12.16931 | P= | 11.76136 |
| w = | 8.177778 | w = | 7.700893 | w = | 7.285068 | w = | 6.921296 | w = | 6.602871 | w = | 6.325 | w = | 6.084656 | w = | 5.880682 |



| d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | d | # hinges: | | |
|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|-------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|----------------|
| 0 | | 0 | | 0 | | 0 | | 0 | | 0 | | 0 | | | |
| 2 | | 2 | | 2 | | 2 | | 2 | | 2 | | 2 | | | |
| 4 | | 4 | | 4 | | 4 | | 4 | | 2 | | 0 | | | |
| 6 | | 6 | | 6 | | 6 | | 4 | | 2 | | 0 | | | |
| 8 | | 8 | | 8 | | 8 | | 4 | | 2 | | 0 | | | |
| 10 | | 10 | | 10 | | 8 | | 4 | | 2 | | 0 | | | |
| 12 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 14 | | 12 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 10 | | 10 | | 10 | | 8 | | 6 | | 4 | | 0 | | | |
| 8 | | 8 | | 8 | | 8 | | 6 | | 4 | | 0 | | | |
| 6 | | 6 | | 6 | | 6 | | 6 | | 4 | | 0 | | | |
| 4 | | 4 | | 4 | | 4 | | 4 | | 4 | | 0 | | | |
| 2 | | 2 | | 2 | | 2 | | 2 | | 2 | | 0 | | | |
| 0 | | 0 | | 0 | | 0 | | 0 | | 0 | | 0 | | | |
| 32 | 28 | 24 | 20 | 16 | 12 | 8 | 4 | | | | | | | | |
| $\delta_{ext} = P*\theta^*$ | 322 | $\delta_{ext} = P*\theta^*$ | 288 | $\delta_{ext} = P*\theta^*$ | 250 | $\delta_{ext} = P*\theta^*$ | 208 | $\delta_{ext} = P*\theta^*$ | 162 | $\delta_{ext} = P*\theta^*$ | 112 | $\delta_{ext} = P*\theta^*$ | 58 | $\delta_{ext} = P*\theta^*$ | 0 |
| $\delta_{ext} = \theta^*$ | 3680 | $\delta_{ext} = \theta^*$ | 3220 | $\delta_{ext} = \theta^*$ | 2760 | $\delta_{ext} = \theta^*$ | 2300 | $\delta_{ext} = \theta^*$ | 1840 | $\delta_{ext} = \theta^*$ | 1380 | $\delta_{ext} = \theta^*$ | 920 | $\delta_{ext} = \theta^*$ | 460 |
| P= | 11.42857 | P= | 11.18056 | P= | 11.04 | P= | 11.05769 | P= | 11.35802 | P= | 12.32143 | P= | 15.86207 | P= | #DIV/0! |
| w = | 5.714286 | w = | 5.590278 | w = | 5.52 | w = | 5.528846 | w = | 5.679012 | w = | 6.160714 | w = | 7.931034 | w = | #DIV/0! |
| | | | | *least upper bound | | | | | | | | | | | |

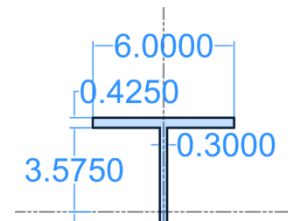
A.4 axial force check on cellular beam

$$w_{failure\ mechanism} = 5.52 \frac{k}{ft} \text{ and } F = \frac{M}{d} \frac{\left(5.52 \frac{k}{ft}\right) (60\ ft)^2}{\frac{8}{26''}} = 95.5\ k$$

top T flange

$$A = (0.425)(6) + (3.575)(0.3) = 3.6225\ in^2$$

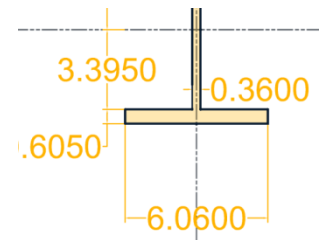
$$\sigma = \frac{F}{A} = \frac{95.5\ k}{3.6225\ in^2} = 26.36\ ksi \leq 50\ ksi$$



Bottom T flange

$$A = (0.605)(6.06) + (3.395)(0.36) = 4.8885\ in^2$$

$$\sigma = \frac{F}{A} = \frac{95.5\ k}{4.8885\ in^2} = 19.54\ ksi \leq 50\ ksi$$



A.5 deflection check on cellular beam

live load deflection

$$\Delta_{LL,allow} = \frac{L}{360} = \frac{(60') \left(12 \frac{in}{ft}\right)}{360} = 2\ in$$

$$\Delta_{LL} \approx \frac{5 \cdot w \cdot L^4}{384 \cdot E \cdot I} = \frac{(5) \left(0.281 \frac{k}{ft}\right) (60\ ft)^4 (12^3)}{(384)(29,000\ ksi)(1433\ in^4)} = 1.97\ in \leq 2\ in \text{ GOOD}$$

$$I = \frac{bh^3}{12} = \left(\frac{(6.03'')(26'')^3}{12}\right) - 2 \cdot \left(\frac{(2.85'')(24.97'')^3}{12} + (2.85)(24.97)(0.18'')^2\right) = 1433\ in^4$$

total load deflection

$$\Delta_{TL,allow} = \frac{L}{240} = \frac{(60') \left(12 \frac{in}{ft}\right)}{240} = 3\ in$$

$$\Delta_{TL} \approx \frac{5 \cdot w \cdot L^4}{384 \cdot E \cdot I} = \frac{(5) \left(0.846 \frac{k}{ft}\right) (60\ ft)^4 (12^3)}{(384)(29,000\ ksi)(1433\ in^4)} = 5.94\ in - (3''\ camber) = 2.94\ in \leq 3\ in \text{ GOOD}$$

A.6 interaction check

NOTE: these values are taken from the RAM model

Precomposite:

Beam: $V = 3.69$ kips $M = 196.09$ kip-ft at 22.125 ft

Top Tee:

| | | |
|-------------------|-------------------|-------------------------------|
| $f_a = 25.68$ ksi | $f_b = 3.98$ ksi | H1-1: $0.869 + 0.113 = 0.982$ |
| $F_a = 29.54$ ksi | $F_b = 30.00$ ksi | H1-2: $0.856 + 0.133 = 0.988$ |

Beam: $V = 5.79$ kips $M = 174.76$ kip-ft at 17.625 ft

Bot Tee:

| | | |
|-------------------|-------------------|-------------------------------|
| $f_a = 16.89$ ksi | $f_b = 6.58$ ksi | |
| $F_t = 30.00$ ksi | $F_b = 30.00$ ksi | H2-1: $0.563 + 0.219 = 0.782$ |

Composite: $V_c = 10.75$ kips

Beam: $V = 21.91$ kips $M = 97.58$ kip-ft at 4.125 ft

Top Tee:

| | | |
|-------------------|-------------------|-------------------------------|
| $f_a = 5.63$ ksi | $f_b = 12.03$ ksi | H1-1: $0.191 + 0.341 = 0.532$ |
| $F_a = 29.54$ ksi | $F_b = 30.00$ ksi | H1-2: $0.188 + 0.401 = 0.589$ |

Beam: $V = 0.95$ kips $M = 380.50$ kip-ft at 28.875 ft

Bot Tee:

| | | |
|-------------------|-------------------|-------------------------------|
| $f_a = 31.88$ ksi | $f_b = 0.00$ ksi | |
| $F_t = 33.00$ ksi | $F_b = 33.00$ ksi | H2-1: $0.966 + 0.000 = 0.966$ |

A.7 web post buckling

NOTE: these values are taken from the RAM model

Precomposite Max $V_h = 12.21$ kips at 2.88 ft

| | Mmax kip-ft | Mallow kip-ft | Mmax/Mallow |
|------|----------------|------------------|-------------|
| Top: | 8.24 | 12.84 | 0.642 |
| Bot: | 8.24 | 16.37 | 0.503 |

Composite Max $V_h = 19.00$ kips at 2.88 ft

| | Mmax kip-ft | Mallow kip-ft | Mmax/Mallow |
|------|----------------|------------------|-------------|
| Top: | 12.82 | 12.84 | 0.999 |
| Bot: | 12.82 | 16.37 | 0.783 |

Therefore, web post buckling controls the section of cellular beam selected

A.8 cellular beam cost analysis

30'x30' composite beam and slab system = **\$17.30¹⁹**

Assembly B10102564200

Based on National Average Costs

Floor, composite metal deck, shear connectors, 5.5" slab, 30'x30' bay, 23.5" total depth, 40 PSF superimposed load, 81 PSF total load

| Description | Quantity | Unit | Material | Installation | Total |
|---|----------|--------|----------------|---------------|----------------|
| Shores, vertical members, to 10' high, includes erect and strip by hand | 0.01500 | Ea. | 0.00 | 0.30 | 0.30 |
| Welded wire fabric, sheets, 6 x 6 - W1.4 x W1.4 (10 x 10) 121 lb. per C.S.F., A185, incl... | 0.01000 | C.S.F. | 0.15 | 0.36 | 0.51 |
| Structural concrete, placing, elevated slab, pumped, less than 6" thick, includes strike... | 0.33300 | C.F. | 0.00 | 0.51 | 0.51 |
| Structural concrete, ready mix, lightweight, 110 #/C.F., 3000 psi, includes local aggre... | 0.33300 | C.F. | 2.41 | 0.00 | 2.41 |
| Concrete finishing, floors, for specified Random Access Floors in ACI Classes 1, 2, 3 an... | 1.00000 | S.F. | 0.00 | 0.86 | 0.86 |
| Concrete surface treatment, curing, sprayed membrane compound | 0.01000 | C.S.F. | 0.08 | 0.09 | 0.17 |
| Weld shear connector, 3/4" dia x 4-7/8" L | 0.12600 | Ea. | 0.09 | 0.25 | 0.35 |
| Structural steel project, apartment, nursing home, etc, 100-ton project, 3 to 6 stories,... | 4.45400 | Lb. | 6.24 | 1.92 | 8.15 |
| Metal floor decking, steel, non-cellular, composite, galvanized, 3" D, 22 gauge | 1.05000 | S.F. | 2.08 | 0.98 | 3.06 |
| Metal decking, steel edge closure form, galvanized, with 2 bends, 12" wide, 18 gauge | 0.03300 | L.F. | 0.13 | 0.08 | 0.21 |
| Sprayed fireproofing, cementitious, normal density, beams, 1 hour rated, 1-3/8" thick... | 0.50400 | S.F. | 0.29 | 0.50 | 0.79 |
| Total | | | \$11.45 | \$5.85 | \$17.30 |

Assuming that the only change from this system is the replacement of W-shape with cellular beams, we have:

@ 60' span, expect SmartBEAM (LB27x35/46) to cost \$150/ton more than traditional W-shape²⁰

LB27x35/46 typical beam size, 3 beams per 30'x60' bay

$$\frac{35+46}{2} = 40.5 \text{ PLF } (60') \cdot (3\text{bms}) = 7290\# = 3.65 \text{ tons}$$

Since the bay size is double the typical bay (30'x30'), divide tonnage by two

$$\frac{3.65 \text{ tons}}{2} = \left(\frac{1.82 \text{ tons}}{30' \times 30' \text{ bay}} \right) \times \left(\frac{\$150}{\text{ton}} \right) = \frac{\$273}{30' \times 30' \text{ bay}}$$

$$\frac{\$273}{900 \text{ SF}} = +\$0.30 \text{ per SF} \times (152,000 \text{ SF}) \approx \$46,200 \text{ total additional cost}$$

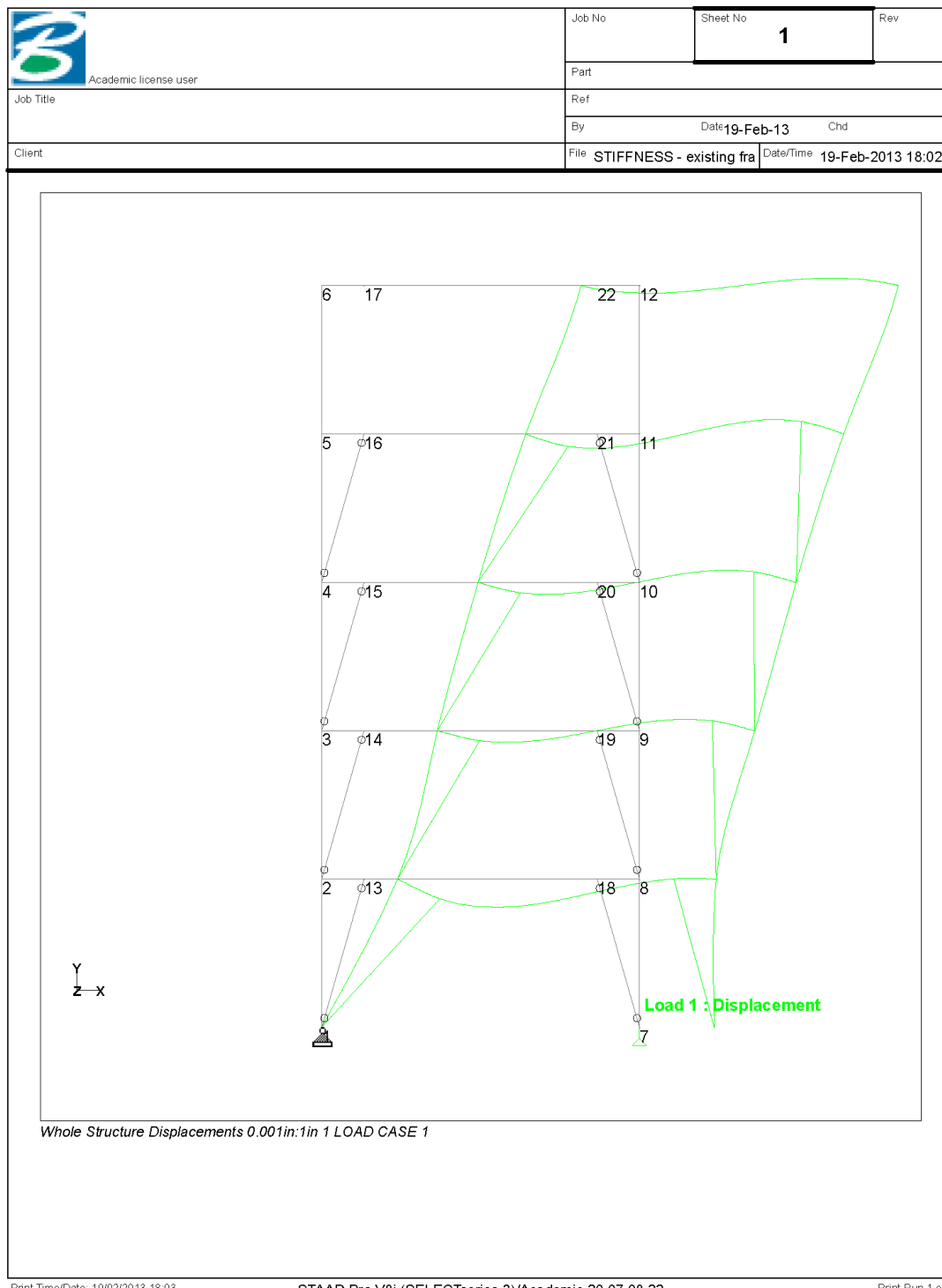
\$17.30 + \$0.30 = \$17.60 Total Cost per SF

¹⁹ "RSMeansOnline," Reed Construction Data Inc., 2013 <meanscostworks.com> (12 October 2012)

²⁰ Steve Redman, CMC Steel, Personal communication (21 March 2013).

appendix B: lateral analysis

B.1 existing frame stiffness calculation



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STAAD.Pro V8i (SELECTSeries 3)/Academic 20.07.08.22

Print Run 1 of 2



| | | | |
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|  Academic license user | Job No | Sheet No 2 | Rev |
| | Part | | |
| Job Title | Ref | | |
| | By | Date: 19-Feb-13 | Chd |
| Client | File: STIFFNESS - existing fra | Date/Time | 19-Feb-2013 18:02 |

Node Displacements

| Node | L/C | X (in) | Y (in) | Z (in) | Resultant (in) | rX (rad) | rY (rad) | rZ (rad) |
|------|-------------|-----------|-----------|-----------|-------------------|-------------|-------------|-------------|
| 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| 2 | 1:LOAD CASE | 0.086 | -0.000 | 0.000 | 0.086 | 0.000 | 0.000 | -0.000 |
| 3 | 1:LOAD CASE | 0.131 | -0.000 | 0.000 | 0.131 | 0.000 | 0.000 | -0.000 |
| 4 | 1:LOAD CASE | 0.177 | -0.000 | 0.000 | 0.177 | 0.000 | 0.000 | -0.000 |
| 5 | 1:LOAD CASE | 0.231 | -0.000 | 0.000 | 0.231 | 0.000 | 0.000 | -0.000 |
| 6 | 1:LOAD CASE | 0.294 | -0.000 | 0.000 | 0.294 | 0.000 | 0.000 | -0.000 |
| 7 | 1:LOAD CASE | 0.085 | 0.000 | 0.000 | 0.085 | 0.000 | 0.000 | 0.000 |
| 8 | 1:LOAD CASE | 0.087 | -0.000 | 0.000 | 0.087 | 0.000 | 0.000 | -0.000 |
| 9 | 1:LOAD CASE | 0.130 | -0.001 | 0.000 | 0.130 | 0.000 | 0.000 | -0.000 |
| 10 | 1:LOAD CASE | 0.177 | -0.000 | 0.000 | 0.177 | 0.000 | 0.000 | -0.000 |
| 11 | 1:LOAD CASE | 0.231 | -0.000 | 0.000 | 0.231 | 0.000 | 0.000 | -0.000 |
| 12 | 1:LOAD CASE | 0.293 | -0.000 | 0.000 | 0.293 | 0.000 | 0.000 | -0.000 |
| 13 | 1:LOAD CASE | 0.086 | -0.023 | 0.000 | 0.089 | 0.000 | 0.000 | -0.000 |
| 14 | 1:LOAD CASE | 0.131 | -0.012 | 0.000 | 0.131 | 0.000 | 0.000 | -0.000 |
| 15 | 1:LOAD CASE | 0.177 | -0.012 | 0.000 | 0.178 | 0.000 | 0.000 | -0.000 |
| 16 | 1:LOAD CASE | 0.231 | -0.015 | 0.000 | 0.232 | 0.000 | 0.000 | -0.000 |
| 17 | 1:LOAD CASE | 0.294 | -0.008 | 0.000 | 0.294 | 0.000 | 0.000 | -0.000 |
| 18 | 1:LOAD CASE | 0.087 | 0.000 | 0.000 | 0.087 | 0.000 | 0.000 | 0.000 |
| 19 | 1:LOAD CASE | 0.130 | 0.011 | 0.000 | 0.131 | 0.000 | 0.000 | -0.000 |
| 20 | 1:LOAD CASE | 0.177 | 0.012 | 0.000 | 0.178 | 0.000 | 0.000 | -0.000 |
| 21 | 1:LOAD CASE | 0.231 | 0.014 | 0.000 | 0.232 | 0.000 | 0.000 | -0.000 |
| 22 | 1:LOAD CASE | 0.293 | 0.007 | 0.000 | 0.293 | 0.000 | 0.000 | -0.000 |

Node Displacement Summary

| | Node | L/C | X (in) | Y (in) | Z (in) | Resultant (in) | rX (rad) | rY (rad) | rZ (rad) |
|---------|------|-------------|--------------|---------------|--------------|-------------------|--------------|--------------|---------------|
| Max X | 6 | 1:LOAD CASE | 0.294 | -0.000 | 0.000 | 0.294 | 0.000 | 0.000 | -0.000 |
| Min X | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Max Y | 21 | 1:LOAD CASE | 0.231 | 0.014 | 0.000 | 0.232 | 0.000 | 0.000 | -0.000 |
| Min Y | 13 | 1:LOAD CASE | 0.086 | -0.023 | 0.000 | 0.089 | 0.000 | 0.000 | -0.000 |
| Max Z | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Min Z | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Max rX | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Min rX | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Max rY | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Min rY | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Max rZ | 18 | 1:LOAD CASE | 0.087 | 0.000 | 0.000 | 0.087 | 0.000 | 0.000 | 0.000 |
| Min rZ | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.001 |
| Max Rst | 17 | 1:LOAD CASE | 0.294 | -0.008 | 0.000 | 0.294 | 0.000 | 0.000 | -0.000 |

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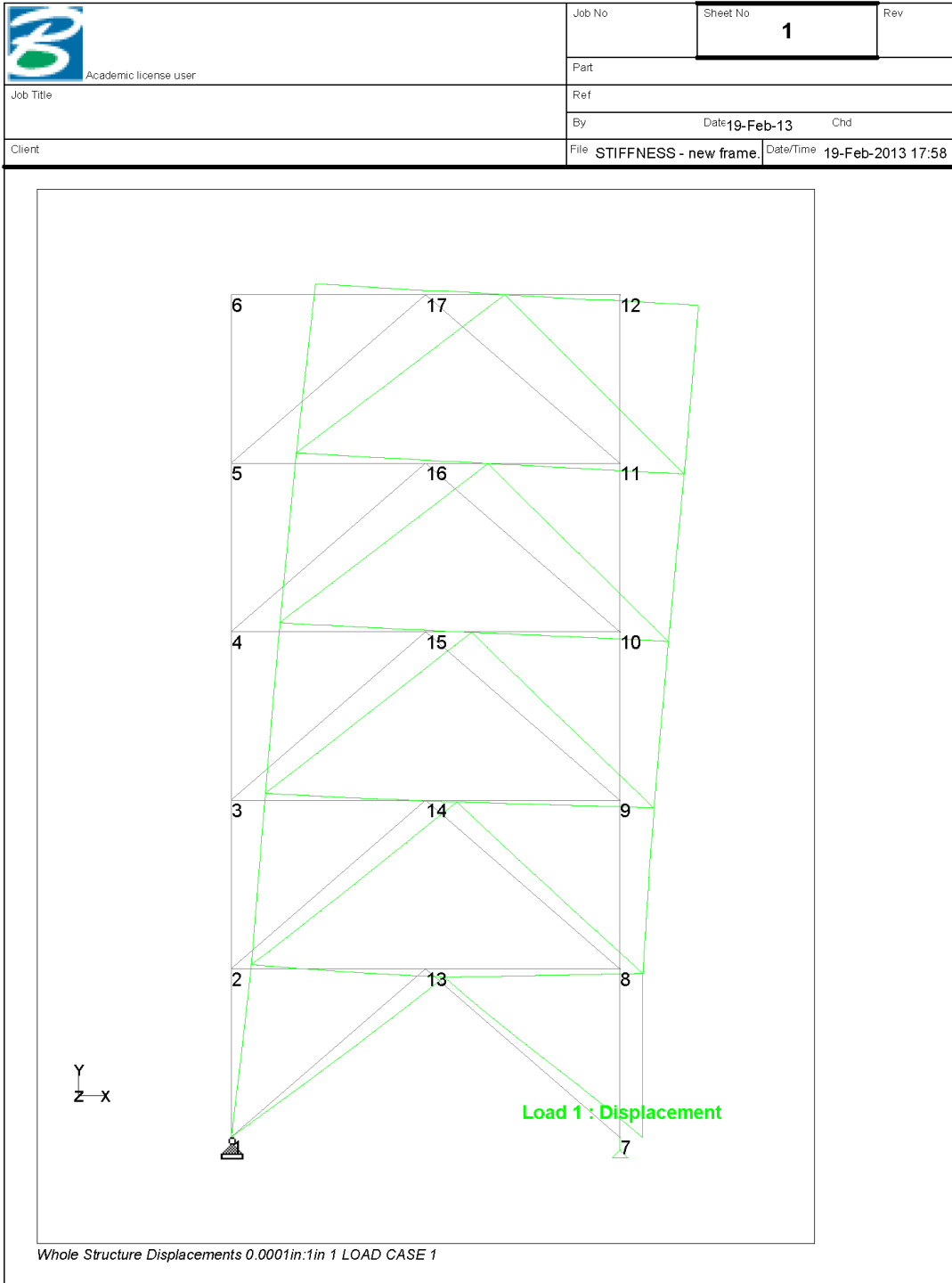
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Print Run 2 of 2

Stiffness of original frame

$$K = \frac{P}{\Delta} = \frac{1 k}{0.294 in} = 3.34 ksi \text{ using STAAD values of displacement}$$

B.2 proposed frame stiffness calculation



| | | | |
|---|------------------------------|------------------------------|-----|
|  Academic license user | Job No | Sheet No 2 | Rev |
| | Part | | |
| Job Title | Ref | | |
| Client | By | Date: 19-Feb-13 | Chd |
| | File: STIFFNESS - new frame. | Date/Time: 19-Feb-2013 17:58 | |

Node Displacements

| Node | L/C | X (in) | Y (in) | Z (in) | Resultant (in) | rX (rad) | rY (rad) | rZ (rad) |
|------|-------------|--------|--------|--------|----------------|----------|----------|----------|
| 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 2 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 3 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 4 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 5 | 1:LOAD CASE | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| 6 | 1:LOAD CASE | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| 7 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 8 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 9 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 10 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 11 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| 12 | 1:LOAD CASE | 0.001 | -0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| 13 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 14 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 15 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 16 | 1:LOAD CASE | 0.000 | -0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| 17 | 1:LOAD CASE | 0.001 | -0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |

Node Displacement Summary

| | Node | L/C | X (in) | Y (in) | Z (in) | Resultant (in) | rX (rad) | rY (rad) | rZ (rad) |
|---------|------|-------------|--------------|---------------|--------------|----------------|--------------|--------------|---------------|
| Max X | 6 | 1:LOAD CASE | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| Min X | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Max Y | 6 | 1:LOAD CASE | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| Min Y | 12 | 1:LOAD CASE | 0.001 | -0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |
| Max Z | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Min Z | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Max rX | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Min rX | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Max rY | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Min rY | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Max rZ | 7 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Min rZ | 1 | 1:LOAD CASE | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.000 |
| Max Rst | 6 | 1:LOAD CASE | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | -0.000 |

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Print Run 2 of 2

Stiffness of proposed frame

$$K = \frac{P}{\Delta} = \frac{1 \text{ k}}{0.1 \text{ in}} = 10 \text{ ksi using STAAD values of displacement}$$

B.3 story displacement load cases/combo

allowable inter-story drift

$$\frac{H}{400} = \frac{(13 \text{ ft}) \left(12 \frac{\text{in}}{\text{ft}}\right)}{400} = 0.39 \text{ in} \geq 0.23398 \text{ in maximum in RAM model, OK}$$

load case definitions

| | | | |
|----|----|-----------------|-----------------|
| 1 | D | DeadLoad | RAMUSER |
| 2 | Lp | PosLiveLoad | RAMUSER |
| 3 | Sp | PosRoofLiveLoad | RAMUSER |
| 4 | E1 | Wind | EQ_IBC09_X_+E_F |
| 5 | E2 | Wind | EQ_IBC09_X_-E_F |
| 6 | E3 | Wind | EQ_IBC09_Y_+E_F |
| 7 | E4 | Wind | EQ_IBC09_Y_-E_F |
| 8 | E5 | Seismic | EQ_IBC09_X_+E_F |
| 9 | E6 | Seismic | EQ_IBC09_X_-E_F |
| 10 | E7 | Seismic | EQ_IBC09_Y_+E_F |
| 11 | E8 | Seismic | EQ_IBC09_Y_-E_F |
| 12 | W1 | Wind Calc X | W_User |
| 13 | W2 | Wind Calc Y | W_User |

load combinations

| | |
|------|--|
| 1 * | 1.000 D |
| 2 * | 1.000 D + 1.000 Lp |
| 3 * | 1.000 D + 1.000 Sp |
| 4 * | 1.000 D + 0.750 Lp + 0.750 Sp |
| 5 * | 1.000 D + 1.000 W1 |
| 6 * | 1.000 D + 1.000 W2 |
| 7 * | 1.000 D - 1.000 W1 |
| 8 * | 1.000 D - 1.000 W2 |
| 9 * | 1.000 D + 0.750 Lp + 0.750 Sp + 0.750 W1 |
| 10 * | 1.000 D + 0.750 Lp + 0.750 Sp + 0.750 W2 |
| 11 * | 1.000 D + 0.750 Lp + 0.750 Sp - 0.750 W1 |
| 12 * | 1.000 D + 0.750 Lp + 0.750 Sp - 0.750 W2 |
| 13 * | 1.000 D + 0.750 Lp + 0.750 W1 |
| 14 * | 1.000 D + 0.750 Lp + 0.750 W2 |
| 15 * | 1.000 D + 0.750 Lp - 0.750 W1 |
| 16 * | 1.000 D + 0.750 Lp - 0.750 W2 |
| 17 * | 1.000 D + 0.750 Sp + 0.750 W1 |
| 18 * | 1.000 D + 0.750 Sp + 0.750 W2 |
| 19 * | 1.000 D + 0.750 Lp - 0.525 E1 |

| | |
|------|--|
| 20 * | 1.000 D + 0.750 Sp - 0.750 W2 |
| 21 * | 0.600 D + 1.000 W1 |
| 22 * | 0.600 D + 1.000 W2 |
| 23 * | 0.600 D - 1.000 W1 |
| 24 * | 0.600 D - 1.000 W2 |
| 25 * | 1.012 D + 0.700 E1 |
| 26 * | 1.012 D + 0.700 E2 |
| 27 * | 1.012 D + 0.700 E3 |
| 28 * | 1.012 D + 0.700 E4 |
| 29 * | 1.012 D + 0.700 E5 |
| 30 * | 1.012 D + 0.700 E6 |
| 31 * | 1.012 D + 0.700 E7 |
| 32 * | 1.012 D + 0.700 E8 |
| 33 * | 1.012 D - 0.700 E1 |
| 34 * | 1.012 D - 0.700 E2 |
| 35 * | 1.012 D - 0.700 E3 |
| 36 * | 1.012 D - 0.700 E4 |
| 37 * | 1.012 D - 0.700 E5 |
| 38 * | 1.012 D - 0.700 E6 |
| 39 * | 1.012 D - 0.700 E7 |
| 40 * | 1.012 D - 0.700 E8 |
| 41 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E1 |
| 42 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E2 |
| 43 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E3 |
| 44 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E4 |
| 45 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E5 |
| 46 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E6 |
| 47 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E7 |
| 48 * | 1.009 D + 0.750 Lp + 0.750 Sp + 0.525 E8 |
| 49 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E1 |
| 50 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E2 |
| 51 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E3 |
| 52 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E4 |
| 53 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E5 |
| 54 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E6 |
| 55 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E7 |
| 56 * | 1.009 D + 0.750 Lp + 0.750 Sp - 0.525 E8 |
| 57 * | 1.009 D + 0.750 Lp + 0.525 E1 |
| 58 * | 1.009 D + 0.750 Lp + 0.525 E2 |
| 59 * | 1.009 D + 0.750 Lp + 0.525 E3 |
| 60 * | 1.009 D + 0.750 Lp + 0.525 E4 |
| 61 * | 1.009 D + 0.750 Lp + 0.525 E5 |
| 62 * | 1.009 D + 0.750 Lp + 0.525 E6 |
| 63 * | 1.009 D + 0.750 Lp + 0.525 E7 |

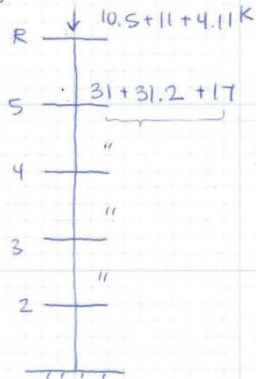
| | |
|-------|-------------------------------|
| 64 * | 1.009 D + 0.750 Lp + 0.525 E8 |
| 65 * | 1.009 D + 0.750 Lp - 0.525 E1 |
| 66 * | 1.009 D + 0.750 Lp - 0.525 E2 |
| 67 * | 1.009 D + 0.750 Lp - 0.525 E3 |
| 68 * | 1.009 D + 0.750 Lp - 0.525 E4 |
| 69 * | 1.009 D + 0.750 Lp - 0.525 E5 |
| 70 * | 1.009 D + 0.750 Lp - 0.525 E6 |
| 71 * | 1.009 D + 0.750 Lp - 0.525 E7 |
| 72 * | 1.009 D + 0.750 Lp - 0.525 E8 |
| 73 * | 1.009 D + 0.750 Sp + 0.525 E1 |
| 74 * | 1.009 D + 0.750 Sp + 0.525 E2 |
| 75 * | 1.009 D + 0.750 Sp + 0.525 E3 |
| 76 * | 1.009 D + 0.750 Sp + 0.525 E4 |
| 77 * | 1.009 D + 0.750 Sp + 0.525 E5 |
| 78 * | 1.009 D + 0.750 Sp + 0.525 E6 |
| 79 * | 1.009 D + 0.750 Sp + 0.525 E7 |
| 80 * | 1.009 D + 0.750 Sp + 0.525 E8 |
| 81 * | 1.009 D + 0.750 Sp - 0.525 E1 |
| 82 * | 1.009 D + 0.750 Sp - 0.525 E2 |
| 83 * | 1.009 D + 0.750 Sp - 0.525 E3 |
| 84 * | 1.009 D + 0.750 Sp - 0.525 E4 |
| 85 * | 1.009 D + 0.750 Sp - 0.525 E5 |
| 86 * | 1.009 D + 0.750 Sp - 0.525 E6 |
| 87 * | 1.009 D + 0.750 Sp - 0.525 E7 |
| 88 * | 1.009 D + 0.750 Sp - 0.525 E8 |
| 89 * | 0.588 D + 0.700 E1 |
| 90 * | 0.588 D + 0.700 E2 |
| 91 * | 0.588 D + 0.700 E3 |
| 92 * | 0.588 D + 0.700 E4 |
| 93 * | 0.588 D + 0.700 E5 |
| 94 * | 0.588 D + 0.700 E6 |
| 95 * | 0.588 D + 0.700 E7 |
| 96 * | 0.588 D + 0.700 E8 |
| 97 * | 0.588 D - 0.700 E1 |
| 98 * | 0.588 D - 0.700 E2 |
| 99 * | 0.588 D - 0.700 E3 |
| 100 * | 0.588 D - 0.700 E4 |
| 101 * | 0.588 D - 0.700 E5 |
| 102 * | 0.588 D - 0.700 E6 |
| 103 * | 0.588 D - 0.700 E7 |
| 104 * | 0.588 D - 0.700 E8 |

appendix C: foundation loads

IMPACT ON FOUNDATIONS @ B2, B9, D2, D9, F2, F9

EDGE COL (B2, F2, B9, F9)

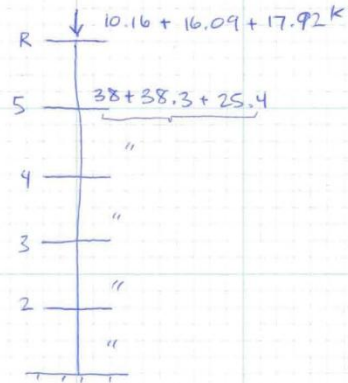
existing loads



TOTAL LOAD = 342.4 k

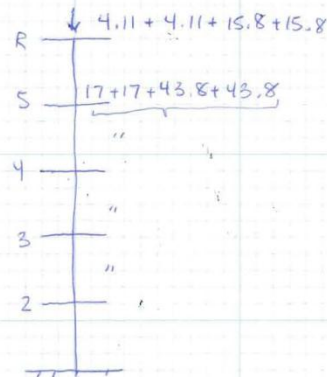
$$\Rightarrow \frac{443.2}{342.4} = 1.3 = 30\% \text{ increase in load on col/foundation}$$

redesign loads



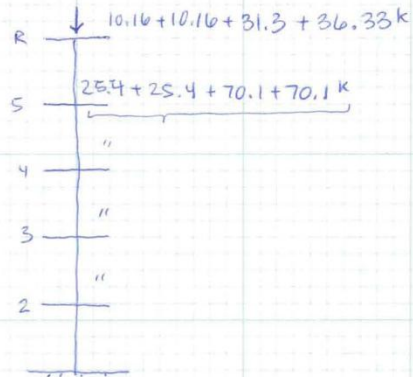
TOTAL LOAD = 443.2 k

MIDDLE COL (D2, D9)



TOTAL LOAD = 526 k

$$\Rightarrow \frac{857}{526} = 1.63 = 63\% \text{ increase in load on foundation}$$



TOTAL LOAD = 857 k



appendix D: architectural calcs

D.1 mullion design

MULLION DESIGN $\frac{1}{2}$

WIND LOAD: $22 \text{ PSF} \times 5' = 110 \text{ PLF}$

$$110 \text{ PLF} \times \frac{1 \text{ FT}}{0.3048 \text{ m}} \times \frac{4.45 \text{ N}}{1 \text{ \#}} = 1.61 \text{ kN/m}$$

ASSUME: MULLION IS ALUMINUM 6063-T5
EXP JOINTS ARE RIGID

BENDING:

$13' = 3.96 \text{ m}$

$$+M_{\max} = \alpha_m \cdot q \cdot L^2$$

$$= (0.0703)(1.61 \text{ kN/m})(3.96 \text{ m})^2$$

$$= \underline{1.77 \text{ kN}\cdot\text{m}}$$

$$-M_{\max} = \alpha_m \cdot q \cdot L^2$$

$$= (-0.125)(1.61)(3.96)^2$$

$$= \underline{-3.16 \text{ kN}\cdot\text{m}}$$

$\therefore -M_{\max} = -3.16 \text{ kN}\cdot\text{m}$ CONTROLS

$$\sigma = \frac{Mc}{I} = \frac{M}{S} \Rightarrow S = \frac{M}{\sigma}$$

$$S = \frac{M}{\sigma} = \frac{-3.16 \text{ kN}\cdot\text{m}}{69000 \text{ kN/m}^2} = 4.57 \text{ E-5 m}^3$$

$$= 45,700 \text{ mm}^3$$

$$S \leq \frac{I}{y}$$

$$45700 \text{ mm}^3 \leq \frac{(\frac{1}{12})(101.6 \text{ mm})^4 - (\frac{1}{12})(101.6 - 2t)^4}{(101.6/2)}$$

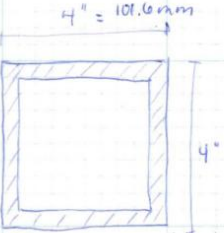
$$2,321,560 + 8879603 = -(\frac{1}{12})(101.6 - 2t)^4$$

$$78696516 = (101.6 - 2t)^4$$

$$94.18 - 101.6 = -2t$$

$$\Rightarrow t = 3.7 = 4 \text{ mm (too thin to make)}$$

\rightarrow try $6.35 \text{ mm} (\approx \frac{1}{4} \text{ "})$



MULLION DESIGN (cont) 2/2

SHEAR:

$$Q_{max} = \alpha_q q L$$

$$= (0.625)(1.61)(3.96)$$

$$= 3.98 \text{ kN}$$

$$T = \left(\frac{3}{2}\right) \frac{V}{A} \Rightarrow A = \left(\frac{3}{2}\right) \frac{V}{T}$$

$$A = \left(\frac{3}{2}\right) \frac{3980 \text{ N}}{37 \text{ N/mm}^2}$$

$$= 157.7 \text{ mm}^2$$

$$157.7 \leq (101.6)^2 - (101.6 - 2t)^2$$

$$100.82 \leq 101.6 - 2t$$

$$0.39 \leq t \quad (\text{again, too small} \rightarrow \text{stick w/ } 6.35 \text{ mm} \sim \frac{1}{4} \text{''})$$

DEFLECTION

$$f_{max} = \frac{\alpha_f q L^4}{100 EI}$$

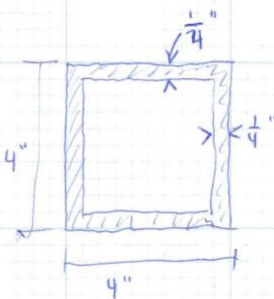
$$= \frac{(0.521)(1.61)(3.96)^4}{100(70000 \text{ N/mm}^2) \left[\left(\frac{1}{12}\right)(101.6)^4 - \left(\frac{1}{12}\right)(101.6 - (6.35)2)^4 \right]}$$

$$= \frac{206.27 \times 10^{12}}{(100)(70000)(8674543)}$$

$$= 8.01 \text{ mm}$$

$$f_{allow} = \frac{SPAN}{180} = \frac{3960 \text{ mm}}{180} = 22 \not\leq 20 \rightarrow \text{use } 20 \text{ mm}$$

$$8.01 \text{ mm} < 20 \text{ mm}, \therefore \text{GOOD!}$$

USE $\frac{1}{4}$ " THICK (6.35mm) MULLION

D.2 R-value + temp gradients

| existing brick veneer wall system | | | | | | |
|-----------------------------------|---------------------------|---------------------|---|---|--|-----------|
| layer material | conductivity, k (W/mK) | thickness, l (m) | conductance, C $C = k/l$ (W/m ² K) | resistance, R _{SI} $R_{SI} = 1/C$ m ² K/W | temp change, ΔT $\Delta T = (R_i/\Sigma R_i) * (T_{int} - T_{ext})$ (°C) | † (°C) |
| exterior temp (-15 C, 85% RH) | | | | | | -15 |
| exterior film | - | - | 34.00 | 0.029 | 0.393 | |
| | | | | | | -14.607 |
| brick | 1.3 | 0.09 | 14.44 | 0.069 | 0.926 | |
| | | | | | | -13.681 |
| air gap | - | 0.04 | - | 0.170 | 2.273 | |
| | | | | | | -11.408 |
| rigid insulation (EPS 1) | 0.039 | 0.05 | 0.78 | 1.282 | 17.144 | |
| | | | | | | 5.736 |
| Batt Insulation/Stud | - | 0.07 | - | 0.896 | 11.981 | |
| | | | | | | 17.717 |
| gypsum board | 0.16 | 0.02 | 8.00 | 0.125 | 1.672 | |
| | | | | | | 19.389 |
| interior film | - | - | 8.30 | 0.120 | 1.611 | |
| interior temp (21 C, 40% RH) | | | | | | 21 |
| | | | | R _{SI} = | 2.692 | |
| | | | | R _{value} = 5.678 * R _{SI} = | 15.286 | |
| | | | | U _{SI} = | 0.371 | |
| | | | | U _{value} = | 0.065 | |

| redesigned insulated panel [brick skin] | | | | | | |
|---|---------------------------|---------------------|---|---|--|-----------|
| layer material | conductivity, k (W/mK) | thickness, l (m) | conductance, C $C = k/l$ (W/m ² K) | resistance, R _{SI} $R_{SI} = 1/C$ m ² K/W | temp change, ΔT $\Delta T = (R_i/\Sigma R_i) * (T_{int} - T_{ext})$ (°C) | † (°C) |
| exterior temp (-15 C, 85% RH) | | | | | | -15 |
| exterior film | - | - | 34.00 | 0.029 | 0.273 | |
| | | | | | | -14.727 |
| brick | 1.3 | 0.09 | 14.44 | 0.069 | 0.643 | |
| | | | | | | -14.084 |
| air gap | - | 0.04 | - | 0.170 | 1.579 | |
| | | | | | | -12.505 |
| insulation panel | - | 0.0508 | - | 2.466 | 22.902 | |
| | | | | | | 10.397 |
| 3" Batt Insulation/6" Stud | - | 0.07 | - | 0.896 | 8.322 | |
| | | | | | | 18.720 |
| gypsum board | 0.16 | 0.02 | 8.00 | 0.125 | 1.161 | |
| | | | | | | 19.881 |
| interior film | - | - | 8.30 | 0.120 | 1.119 | |
| interior temp (21 C, 40% RH) | | | | | | 21 |
| | | | | R _{SI} = | 3.876 | |
| | | | | R _{value} = 5.678 * R _{SI} = | 22.007 | |
| | | | | U _{SI} = | 0.258 | |
| | | | | U _{value} = | 0.045 | |

redesigned insulated panel [metal skin]

| layer material | conductivity, k (W/mK) | thickness, l (m) | conductance, C $C = k/l$ (W/m ² K) | resistance, R _{SI} $R_{SI} = 1/C$ m ² K/W | temp change, ΔT $\Delta T = (R_i/\Sigma R_i) * (T_{int} - T_{ext})$ (°C) | t (°C) |
|--------------------------------------|---------------------------|---------------------|---|---|--|-----------|
| <i>exterior temp (-15 C, 85% RH)</i> | | | | | | |
| exterior film | - | - | 34.00 | 0.029 | 0.278 | |
| | | | | | | -14.722 |
| metal panel | 80 | 0.008 | 10000.00 | 0.000 | 0.001 | |
| | | | | | | -14.721 |
| air gap | - | 0.04 | - | 0.170 | 1.608 | |
| | | | | | | -13.113 |
| insulation panel | 0.039 | 0.0508 | - | 2.466 | 23.318 | |
| | | | | | | 10.205 |
| 3" Batt Insulation/6"Stud | - | 0.07 | - | 0.896 | 8.474 | |
| | | | | | | 18.678 |
| gypsum board | 0.16 | 0.02 | 8.00 | 0.125 | 1.182 | |
| | | | | | | 19.861 |
| interior film | - | - | 8.30 | 0.120 | 1.139 | |
| <i>interior temp (21 C, 40% RH)</i> | | | | | | |

| | |
|--------------------------------|---------------|
| $R_{SI} =$ | 3.807 |
| $R_{value} = 5.678 * R_{SI} =$ | 21.614 |
| $U_{SI} =$ | 0.263 |
| $U_{value} =$ | 0.046 |

D.3 pressure gradient + RH

| existing brick veneer wall system | | | | | | | |
|-----------------------------------|---|--|---|--|------------------------------|---|-------------------------------------|
| layer material | permeability, μ permeability, μ (ng/Pa*s*m) | permeance, M $M = \mu/t$ (ng/Pa*s*m ²) | $R_{v,j}$ $R_{v,j} = 1/M$ (Pa*s*m ² /ng) | pressure change, ΔP $\Delta P = (R_{v,j}/\Sigma R_{v,j}) * (P_{int} - P_{ext})$ (Pa) | P_w @ interface (Pa) | $P_{w,sat}$ $P_{w,sat} = 1000e^{(52.58 - 6790.5/T - 5.028 \ln T)}$ (Pa) | RH $RH = P_w / P_{w,sat}$ (%) |
| exterior temp (-15 C, 85% RH) | | | | | 162.43 | 191.1 | 85.0 |
| exterior film | - | 75000 | 0.000013 | 0.163 | 162.6 | 197.4 | 82.4 |
| brick | 10 | 111.11111111 | 0.009000 | 109.864 | 272.5 | 212.9 | 128.0 |
| air gap | | 7200 | 0.000139 | 1.695 | 274.2 | 255.6 | 107.2 |
| rigid insulation (EPS 1) | 2 | 40 | 0.025000 | 305.179 | 579.3 | 913.5 | 63.4 |
| Batt Insulation/Stud | 3 | 42.85714286 | 0.023333 | 284.834 | 864.2 | 2012.8 | 42.9 |
| gypsum board | 2 | 100 | 0.010000 | 122.072 | 986.2 | 2234.3 | 44.1 |
| interior film | - | 15000 | 0.000067 | 0.814 | 987.1 | 2467.6 | 40.0 |
| interior temp (21 C, 40% RH) | | | | | | | |
| | | | 0.067552 | 824.62 | | | |

| redesigned insulated panel [brick skin] | | | | | | | |
|---|---|--|---|--|------------------------------|---|-------------------------------------|
| layer material | permeability, μ permeability, μ (ng/Pa*s*m) | permeance, M $M = \mu/t$ (ng/Pa*s*m ²) | $R_{v,j}$ $R_{v,j} = 1/M$ (Pa*s*m ² /ng) | pressure change, ΔP $\Delta P = (R_{v,j}/\Sigma R_{v,j}) * (P_{int} - P_{ext})$ (Pa) | P_w @ interface (Pa) | $P_{w,sat}$ $P_{w,sat} = 1000e^{(52.58 - 6790.5/T - 5.028 \ln T)}$ (Pa) | RH $RH = P_w / P_{w,sat}$ (%) |
| exterior temp (-15 C, 85% RH) | | | | | 162.4310376 | 191.1 | 85.0 |
| exterior film | - | 75000 | 0.000013 | 0.161804 | 162.592842 | 195.4 | 83.2 |
| brick | 10 | 111.1 | 0.009000 | 109.217666 | 271.810507 | 206.0 | 131.9 |
| air gap | | 7200 | 0.000139 | 1.685458 | 273.495965 | 234.1 | 116.8 |
| insulation panel | 2 | 39.37 | 0.025400 | 308.236524 | 581.732489 | 1253.4 | 46.4 |
| Batt Insulation/Stud | 3 | 42.86 | 0.023333 | 283.156911 | 864.889400 | 2143.2 | 40.4 |
| gypsum board | 2 | 100 | 0.010000 | 121.352962 | 986.242362 | 2303.4 | 42.8 |
| interior film | - | 15000 | 0.000067 | 0.809020 | 987.051 | 2467.6 | 40.0 |
| interior temp (21 C, 40% RH) | | | | | | | |
| | | | 0.067952 | 824.62 | | | |

| redesigned insulated panel [metal skin] | | | | | | | |
|---|---|--|---|--|------------------------------|---|-------------------------------------|
| layer material | permeability, μ permeability, μ (ng/Pa*s*m) | permeance, M $M = \mu/t$ (ng/Pa*s*m ²) | $R_{v,j}$ $R_{v,j} = 1/M$ (Pa*s*m ² /ng) | pressure change, ΔP $\Delta P = (R_{v,j}/\Sigma R_{v,j}) * (P_{int} - P_{ext})$ (Pa) | P_w @ interface (Pa) | $P_{w,sat}$ $P_{w,sat} = 1000e^{(52.58 - 6790.5/T - 5.028 \ln T)}$ (Pa) | RH $RH = P_w / P_{w,sat}$ (%) |
| exterior temp (-15 C, 85% RH) | | | | | 162.43 | 191.1 | 85.0 |
| exterior film | - | 75000 | 0.000013 | 0.184 | 162.6 | 195.5 | 83.2 |
| metal panel | 10 | 1250 | 0.000800 | 11.041 | 173.7 | 195.5 | 88.8 |
| air gap | | 7200 | 0.000139 | 1.917 | 175.6 | 222.9 | 78.8 |
| insulation panel | 2 | 39.37007874 | 0.025400 | 350.537 | 526.1 | 1237.5 | 42.5 |
| Batt Insulation/Stud | 3 | 42.85714286 | 0.023333 | 322.015 | 848.1 | 2137.7 | 39.7 |
| gypsum board | 2 | 100 | 0.010000 | 138.007 | 986.1 | 2300.5 | 42.9 |
| interior film | - | 15000 | 0.000067 | 0.920 | 987.1 | 2467.6 | 40.0 |
| interior temp (21 C, 40% RH) | | | | | | | |
| | | | 0.059752 | 824.62 | | | |

appendix E: mechanical calcs

E.1 HVAC loads for typical floor

| HVAC Loads for Typical Floor | | | | | | | |
|------------------------------|-----------|----------------------|-------------------|------------------|------------------|--------------|--------------|
| Room Name | Area (sf) | Lighting Load (W/sf) | Misc. Load (W/sf) | Number of People | Total Load (btu) | CFM Required | Adjusted CFM |
| 220 Office | 240 | 1.0 | 0.83 | 1 | 1757 | 80 | 75 |
| 302 Conference | 290 | 1.0 | 6.90 | 10 | 10366 | 471 | 475 |
| 304 Copy | 130 | 1.0 | 0.00 | 0 | 444 | 20 | 25 |
| 306 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 308 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 310 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 312 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 320 Conference | 430 | 1.0 | 6.51 | 14 | 14594 | 663 | 675 |
| 322 Kitchen | 330 | 1.0 | 4.85 | 8 | 8627 | 392 | 400 |
| 324 Conference | 430 | 1.0 | 6.51 | 14 | 14594 | 663 | 675 |
| 330 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 332 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 334 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 336 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 338 Copy | 110 | 1.0 | 0.00 | 0 | 375 | 17 | 25 |
| 420 Office | 250 | 1.0 | 0.80 | 1 | 1791 | 81 | 75 |
| 418 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 416 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 414 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 410 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 408 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 406 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 404 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 402 Office | 250 | 1.0 | 0.80 | 1 | 1791 | 81 | 75 |
| 142 Copy | 110 | 1.0 | 0.00 | 0 | 375 | 17 | 25 |
| 140 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 138 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 136 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 134 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 132 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 130 Office | 160 | 1.0 | 1.25 | 1 | 1484 | 67 | 75 |
| 124 Conference | 400 | 1.0 | 7.00 | 14 | 14492 | 659 | 650 |
| 122 Conference | 260 | 1.0 | 6.15 | 8 | 8388 | 381 | 375 |
| 120 Conference | 410 | 1.0 | 6.83 | 14 | 14526 | 660 | 650 |
| 110 Office | 160 | 1.0 | 1.25 | 1 | 1484 | 67 | 75 |
| 108 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 106 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 104 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 102 Copy | 110 | 1.0 | 0.00 | 0 | 375 | 17 | 25 |
| 202 Office | 240 | 1.0 | 0.83 | 1 | 1757 | 80 | 75 |
| 204 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 206 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 208 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 210 Office | 160 | 1.0 | 1.25 | 1 | 1484 | 67 | 75 |
| 214 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 216 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 218 Office | 160 | 1.0 | 1.25 | 1 | 1484 | 67 | 75 |



| Room Name | Area (sf) | Lighting Load (W/sf) | Misc. Load (W/sf) | Number of People | Total Load (btu) | CFM Required | Adjusted CFM |
|-------------------|-----------|----------------------|-------------------|------------------|------------------|--------------|--------------|
| Open Office NW | 1738 | 1.0 | 1.15 | 10 | 15308 | 696 | 700 |
| 309 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 311 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 510 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 512 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 700 Training Room | 600 | 1.0 | 6.67 | 20 | 20800 | 945 | 950 |
| 560 Conference | 670 | 1.0 | 5.37 | 18 | 19164 | 871 | 875 |
| 800 File Room | 600 | 1.0 | 0.00 | 0 | 2048 | 93 | 100 |
| 329 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 331 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 530 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 532 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| Open Office NE | 2442 | 1.0 | 1.06 | 13 | 20523 | 933 | 925 |
| Open Office SW | 1800 | 1.0 | 1.44 | 13 | 18332 | 833 | 825 |
| 609 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 607 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 605 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 603 Office | 160 | 1.0 | 1.25 | 1 | 1484 | 67 | 75 |
| 107 ITS Server | 570 | 1.0 | 0.00 | 0 | 1945 | 88 | 100 |
| 107a Storage | 240 | 1.0 | 0.00 | 0 | 819 | 37 | 25 |
| 111 Guest Office | 80 | 1.0 | 2.50 | 1 | 1211 | 55 | 50 |
| 001 Elev Lobby | 610 | 1.0 | 0.00 | 0 | 2082 | 95 | 100 |
| 100 Reception | 600 | 1.0 | 2.67 | 8 | 9549 | 434 | 425 |
| 129 Office | 100 | 1.0 | 2.00 | 1 | 1279 | 58 | 50 |
| 131 Guest Office | 100 | 1.0 | 2.00 | 1 | 1279 | 58 | 50 |
| 135 Guest Office | 100 | 1.0 | 2.00 | 1 | 1279 | 58 | 50 |
| 133 Kitchen | 380 | 1.0 | 6.32 | 12 | 12548 | 570 | 575 |
| 909 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 907 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 905 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| 903 Office | 150 | 1.0 | 1.33 | 1 | 1450 | 66 | 75 |
| Open Office SE | 1437 | 1.0 | 1.39 | 10 | 14280 | 649 | 650 |
| 100W Corridor | 400 | 1.0 | 0.00 | 0 | 1365 | 62 | 50 |
| 500W Corridor | 800 | 1.0 | 0.00 | 0 | 2730 | 124 | 125 |
| 500 Corridor | 500 | 1.0 | 0.00 | 0 | 1707 | 78 | 75 |
| 300 Corridor | 700 | 1.0 | 0.00 | 0 | 2389 | 109 | 100 |
| 700n Corridor | 191 | 1.0 | 0.00 | 0 | 652 | 30 | 25 |
| 800n Corridor | 210 | 1.0 | 0.00 | 0 | 717 | 33 | 25 |
| 100e Corridor | 315 | 1.0 | 0.00 | 0 | 1075 | 49 | 50 |

| TOTALS | |
|------------------|--------------|
| Square Footage | 26423 |
| CFM Required | 14800 |
| CFM/SF | 0.56 |
| Total Population | 100 |
| Population Div. | 41.3% |

E.2 ASHRAE 62.1-2007 outdoor air requirements

| Ventilation for Acceptable Indoor Air Quality (ASHRAE 62.1-2007) | | | | | | | | | | |
|--|-----------|----------------------|----------------------|--------------------|-----------|----------------------------|-------------------------------|----------------|-------------------------------|------|
| Program Area (SF) | Room Type | People | Area | Occupant | Air Class | Zone | Breathing | Zone OA, | | |
| | | Outdoor Air Rate, Rp | Outdoor Air Rate, Ra | Density, #/1000 sf | | Population, P _z | Zone OA, V _{bz, cfm} | E _z | Zone OA, V _{oz, cfm} | |
| 220 Office | 240 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 19.4 | 1.0 | 19.4 |
| 302 Conference | 290 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 10 | 67.4 | 1.0 | 67.4 |
| 304 Copy | 130 | Storage Rooms | 0 | 0.12 | 0 | 0 | 0 | 15.6 | 1.0 | 15.6 |
| 306 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 308 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 310 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 312 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 320 Conference | 430 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 14 | 95.8 | 1.0 | 95.8 |
| 322 Kitchen | 330 | Office Space | 5 | 0.06 | 5 | 1 | 8 | 59.8 | 1.0 | 59.8 |
| 324 Conference | 430 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 14 | 95.8 | 1.0 | 95.8 |
| 330 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 332 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 334 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 336 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 338 Copy | 110 | Storage Rooms | 0 | 0.12 | 0 | 0 | 0 | 13.2 | 1.0 | 13.2 |
| 420 Office | 250 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 20 | 1.0 | 20 |
| 418 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 416 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 414 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 410 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 408 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 406 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 404 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 402 Office | 250 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 20 | 1.0 | 20 |
| 142 Copy | 110 | Storage Rooms | 0 | 0.12 | 0 | 0 | 0 | 13.2 | 1.0 | 13.2 |
| 140 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 138 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 136 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 134 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 132 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 130 Office | 160 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14.6 | 1.0 | 14.6 |
| 124 Conference | 400 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 14 | 94 | 1.0 | 94 |
| 122 Conference | 260 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 8 | 55.6 | 1.0 | 55.6 |
| 120 Conference | 410 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 14 | 94.6 | 1.0 | 94.6 |
| 110 Office | 160 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14.6 | 1.0 | 14.6 |
| 108 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 106 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 104 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 102 Copy | 110 | Storage Rooms | 0 | 0.12 | 0 | 0 | 0 | 13.2 | 1.0 | 13.2 |
| 202 Office | 240 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 19.4 | 1.0 | 19.4 |
| 204 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 206 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 208 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 210 Office | 160 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14.6 | 1.0 | 14.6 |
| 214 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 216 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 218 Office | 160 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14.6 | 1.0 | 14.6 |



| Program Area (SF) | Room Type | People | Area | Occupant Density, #/1000 sf | Air Class | Zone Population, P _z | Breathing | | Zone OA, E _z | Zone OA, V _{oz,cfm} |
|-------------------|-----------|------------------------|----------------------|-----------------------------|-----------|---------------------------------|------------------------------|-------------------------|-------------------------|------------------------------|
| | | Outdoor Air Rate, Rp | Outdoor Air Rate, Ra | | | | Zone OA, V _{bz,cfm} | Zone OA, E _z | | |
| Open Office NW | 1738 | Office Space | 5 | 0.06 | 5 | 1 | 10 | 154.28 | 1.0 | 154.28 |
| 309 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 311 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 510 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 512 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 700 Training Room | 600 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 20 | 136 | 1.0 | 136 |
| 560 Conference | 670 | Conference/ meeting | 5 | 0.06 | 50 | 1 | 18 | 130.2 | 1.0 | 130.2 |
| 800 File Room | 600 | Storage Rooms | 0 | 0.12 | 0 | 0 | 0 | 72 | 1.0 | 72 |
| 329 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 331 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 530 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 532 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| Open Office NE | 2442 | Office Space | 5 | 0.06 | 5 | 1 | 13 | 211.52 | 1.0 | 211.52 |
| Open Office SW | 1800 | Office Space | 5 | 0.06 | 5 | 1 | 13 | 173 | 1.0 | 173 |
| 609 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 607 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 605 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 603 Office | 160 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14.6 | 1.0 | 14.6 |
| 107 ITS Server | 570 | Electrical Equip Rooms | 0 | 0.06 | 0 | 0 | 0 | 34.2 | 1.0 | 34.2 |
| 107a Storage | 240 | Storage Rooms | 0 | 0.12 | 0 | 0 | 0 | 28.8 | 1.0 | 28.8 |
| 111 Office | 80 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 9.8 | 1.0 | 9.8 |
| 001 Elev Lobby | 610 | Reception Areas | 5 | 0.06 | 5 | 1 | 0 | 36.6 | 1.0 | 36.6 |
| 100 Reception | 600 | Reception Areas | 5 | 0.06 | 5 | 1 | 8 | 76 | 1.0 | 76 |
| 129 Office | 100 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 11 | 1.0 | 11 |
| 131 Office | 100 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 11 | 1.0 | 11 |
| 135 Office | 100 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 11 | 1.0 | 11 |
| 133 Kitchen | 380 | Office Space | 5 | 0.06 | 5 | 1 | 12 | 82.8 | 1.0 | 82.8 |
| 909 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 907 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 905 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| 903 Office | 150 | Office Space | 5 | 0.06 | 5 | 1 | 1 | 14 | 1.0 | 14 |
| Open Office SE | 1437 | Office Space | 5 | 0.06 | 5 | 1 | 10 | 136.22 | 1.0 | 136.22 |
| 100W Corridor | 400 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 24 | 1.0 | 24 |
| 500W Corridor | 800 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 48 | 1.0 | 48 |
| 500 Corridor | 500 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 30 | 1.0 | 30 |
| 300 Corridor | 700 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 42 | 1.0 | 42 |
| 700n Corridor | 191 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 11.46 | 1.0 | 11.46 |
| 800n Corridor | 210 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 12.6 | 1.0 | 12.6 |
| 100e Corridor | 315 | Corridors | 0 | 0.06 | 0 | 1 | 0 | 18.9 | 1.0 | 18.9 |



E.3 TRACE system checksums

System Checksums By ACADEMIC

| Packaged Terminal Air Conditioner | | | | | | | | | | | |
|-----------------------------------|---------------------|-----------|----------------|------------------|------------------|-----------------------|--------------------|------------------|--------------|--------|--------|
| COOLING COIL PEAK | | | CLG SPACE PEAK | | | HEATING COIL PEAK | | | TEMPERATURES | | |
| Peaked at Time: Outside Air: | | | Mo/Hr: 7 / 15 | | | Mo/Hr: Heating Design | | | SADB | | |
| OADB: 86 / 71 / 95 | | | OADB: Peaks | | | OADB: 5 | | | Cooling | | |
| Space Sens. + Lat. | Plenum Sens. + Lat. | Net Total | Space Sensible | Percent Of Total | Percent Of Total | Space Sens | Coil Peak Tot Sens | Percent Of Total | Ra Plenum | Return | Ret/OA |
| Btu/h | Btu/h | Btu/h | Btu/h | (%) | (%) | Btu/h | Btu/h | (%) | 75.0 | 70.0 | 54.1 |
| Envelope Loads | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| SkyLite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| SkyLite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Glass Solar | 20,115 | 0 | 20,115 | 17 | 37 | -10,229 | -10,229 | 8.10 | 76.1 | 70.0 | 54.1 |
| Glass/Door Cond | 718 | 0 | -219 | 1 | 0 | -6,560 | -6,560 | 5.19 | 78.5 | 54.1 | 54.1 |
| Wall Cond | 2,648 | 0 | 2,658 | 2 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Infiltration | 19,816 | 0 | 5,346 | 17 | 7 | -54,828 | -54,828 | 43.39 | 0.0 | 0.0 | 0.0 |
| Sub Total ==> | 43,297 | 0 | 35,137 | 37 | 47 | -71,618 | -71,618 | 56.68 | 0.0 | 0.0 | 0.0 |
| Internal Loads | | | | | | | | | | | |
| Lights | 18,258 | 4,564 | 22,822 | 19 | 25 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| People | 34,878 | 0 | 34,878 | 29 | 28 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Sub Total ==> | 53,136 | 4,564 | 57,700 | 49 | 53 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Ventilation Load | 0 | 0 | 20,017 | 17 | 0 | -54,736 | -54,736 | 43.32 | 0.0 | 0.0 | 0.0 |
| Adj Air Trans Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Exhaust Heat | -2,450 | 0 | -2,450 | -2 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Duct Heat PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Underfir Sup Ht PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | 0.0 |
| Grand Total ==> | 96,433 | 2,114 | 118,564 | 100.00 | 100.00 | 74,275 | -126,354 | 100.00 | 0.0 | 0.0 | 0.0 |

| Packaged Terminal Air Conditioner | | | | | | | | | | | |
|-----------------------------------|-----------|--------------|-------|-------|-------------|------------------------|--------------------|------------------|-----------------|---------|------------|
| COOLING COIL SELECTION | | | AREAS | | | HEATING COIL SELECTION | | | ENGINEERING CKS | | |
| Total Capacity | Sens Cap. | Coil Airflow | Enter | Leave | Gross Total | Space Sens | Coil Peak Tot Sens | Percent Of Total | % OA | cfm/ft² | ft²/ton |
| ton | MBh | cfm | °F | °F | Glass | Btu/h | Btu/h | (%) | cm | cfm/ton | Btu/hr-ft² |
| Main Clg | 9.9 | 118.6 | 80.0 | 53.5 | 6,079 | 0 | 0 | 0.00 | 24.4 | 0.53 | 19.50 |
| Aux Clg | 0.0 | 0.0 | 0.0 | 52.5 | 0 | 0 | 0 | 0.00 | 0.53 | 0.53 | 0.00 |
| Opt Vent | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 9.9 | 118.6 | 80.0 | 52.5 | 6,079 | 0 | 0 | 0.00 | 24.4 | 0.53 | 19.50 |

| Packaged Terminal Air Conditioner | | | | | | | | | |
|-----------------------------------|-----------|--------|----------|----------|----------|-----------------|---------|---------|------------|
| TEMPERATURES | | | AIRFLOWS | | | ENGINEERING CKS | | | |
| SADB | Ra Plenum | Return | Diffuser | Terminal | Main Fan | % OA | cfm/ft² | ft²/ton | Btu/hr-ft² |
| 90.8 | 75.0 | 70.0 | 3.233 | 3.233 | 3.233 | 24.4 | 0.53 | 0.53 | 19.50 |
| 90.8 | 75.0 | 70.0 | 3.233 | 3.233 | 3.233 | 24.4 | 0.53 | 0.53 | 19.50 |
| 70.0 | 76.1 | 70.0 | 3.233 | 3.233 | 3.233 | 0.53 | 0.53 | 0.53 | 0.00 |
| 54.1 | 78.5 | 54.1 | 3.233 | 3.233 | 3.233 | 327.22 | 615.26 | 615.26 | -20.79 |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 19.50 | 0.00 | 0.00 | 0.00 |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 85 | 0.00 | 0.00 | 0.00 |

Project Name: MTOB 1-1,TRC
Dataset Name: MTOB 1-1,TRC

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System Checksums
By ACADEMIC

| AHU-02 | | COOLING COIL PEAK | | | | CLG SPACE PEAK | | | HEATING COIL PEAK | | | Packaged Terminal Air Conditioner | | | |
|------------------------------|---------------------|--------------------------|------------------|----------------|------------------|-----------------------|------------------|-----------------------|-------------------|----------------------|------------|-----------------------------------|------------|------------------|--------------|
| Peaked at Time: Outside Air: | | Mo/Hr: 7 / 15 | | Mo/Hr: Sum of | | Mo/Hr: Heating Design | | Mo/Hr: Heating Design | | | | | | | |
| | | OADB/WB/HR: 86 / 71 / 95 | | OADB: Peaks | | OADB: Peaks | | OADB: 5 | | | | | | | |
| Space Sens. + Lat. | Plenum Sens. + Lat. | Net Total | Percent Of Total | Space Sensible | Percent Of Total | Space Peak | Percent Of Total | Space Peak | Percent Of Total | Envelope Loads | Space Peak | Percent Of Total | Space Peak | Percent Of Total | TEMPERATURES |
| Btu/h | Btu/h | Btu/h | (%) | Btu/h | (%) | Btu/h | (%) | Btu/h | (%) | | Btu/h | (%) | Btu/h | (%) | |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Envelope Loads | 0 | 0.00 | 0 | 0.00 | SADB |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | SkyLite Solar | 0 | 0.00 | 0 | 0.00 | Cooling |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | SkyLite Cond | 0 | 0.00 | 0 | 0.00 | Heating |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Roof Cond | 0 | 0.00 | 0 | 0.00 | 52.3 |
| 24,662 | 0 | 24,662 | 18 | 30,852 | 37 | 30,852 | 37 | -11,161 | 0 | Glass Solar | -11,161 | 7.40 | -11,161 | 7.40 | Ra Plenum |
| -106 | 0 | -106 | 0 | -808 | -1 | -808 | -1 | -7,158 | 0 | Glass/Door Cond | -7,158 | 4.75 | -7,158 | 4.75 | Return |
| 2,491 | 0 | 2,491 | 2 | 2,496 | 3 | 2,496 | 3 | 0 | 0 | Wall Cond | 0 | 0.00 | 0 | 0.00 | Ret/OA |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Partition/Door | 0 | 0.00 | 0 | 0.00 | Fn MrrTD |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Floor | 0 | 0.00 | 0 | 0.00 | Fn BlrTD |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Adjacent Floor | 0 | 0.00 | 0 | 0.00 | Fn Frict |
| 25,243 | 0 | 25,243 | 19 | 6,806 | 8 | 6,806 | 8 | -71,180 | 0 | Infiltration | -71,180 | 47.21 | -71,180 | 47.21 | Cooling |
| 52,288 | 0 | 52,288 | 39 | 39,346 | 47 | 39,346 | 47 | -89,500 | 0 | Sub Total ==> | -89,500 | 59.36 | -89,500 | 59.36 | Heating |
| | | | | | | | | | | Internal Loads | | | | | |
| 23,703 | 5,926 | 29,629 | 22 | 23,703 | 28 | 23,703 | 28 | 0 | 0 | Lights | 0 | 0.00 | 0 | 0.00 | Infil |
| 34,110 | 0 | 34,110 | 25 | 20,203 | 24 | 20,203 | 24 | 0 | 0 | People | 0 | 0.00 | 0 | 0.00 | 1,026 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Misc | 0 | 0.00 | 0 | 0.00 | 883 |
| 57,813 | 5,926 | 63,738 | 47 | 43,906 | 53 | 43,906 | 53 | 0 | 0 | Sub Total ==> | 0 | 0.00 | 0 | 0.00 | 883 |
| | | | | | | | | | | Ceiling Load | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ventilation Load | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Adj Air Trans Heat | 0 | 0.00 | 0 | 0.00 | 1,026 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ov/Undr Sizing | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | -3,305 | -3,305 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | Exhaust Heat | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | RA Preheat Diff. | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Additional Reheat | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Underfir Sup Ht PkUp | 0 | 0.00 | 0 | 0.00 | 883 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Supply Air Leakage | 0 | 0.00 | 0 | 0.00 | 883 |
| 110,100 | 2,621 | 134,364 | 100.00 | 83,251 | 100.00 | 83,251 | 100.00 | -89,500 | -150,767 | Grand Total ==> | -89,500 | 100.00 | -150,767 | 100.00 | AHU Vent |
| | | | | | | | | | | Airflows | | | | | |
| | | | | | | | | | | Diffuser | 3,433 | 3.433 | 3,433 | 3.433 | Terminal |
| | | | | | | | | | | Main Fan | 3,433 | 3.433 | 3,433 | 3.433 | Return |
| | | | | | | | | | | Sec Fan | 0 | 0.00 | 0 | 0.00 | Exhaust |
| | | | | | | | | | | Nom Vent | 883 | 883 | 883 | 883 | Rm Exh |
| | | | | | | | | | | AHU Vent | 883 | 883 | 883 | 883 | Auxiliary |
| | | | | | | | | | | Infil | 1,026 | 1,026 | 1,026 | 1,026 | Leakage Dwn |
| | | | | | | | | | | MinStop/Rh | 0 | 0.00 | 0 | 0.00 | Leakage Ups |
| | | | | | | | | | | Return | 4,459 | 4.459 | 4,459 | 4.459 | 0 |
| | | | | | | | | | | Exhaust | 1,909 | 1.909 | 1,909 | 1.909 | 0 |
| | | | | | | | | | | Sub Total ==> | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Ceiling Load | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Ventilation Load | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Adj Air Trans Heat | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Ov/Undr Sizing | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Exhaust Heat | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | RA Preheat Diff. | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Additional Reheat | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Underfir Sup Ht PkUp | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Supply Air Leakage | 0 | 0.00 | 0 | 0.00 | 0 |
| | | | | | | | | | | Grand Total ==> | -89,500 | -150,767 | -150,767 | -150,767 | 0 |

Project Name: MTOB 1-1,TRC
Dataset Name: MTOB 1-1,TRC
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System Checksums By ACADEMIC

| AHU-03 | | Packaged Terminal Air Conditioner | | | | | | |
|---------------------------------|---|-----------------------------------|----------------------------------|----------------------------|----------------------------|---------------------|--------------------------------|----------------------------|
| COOLING COIL PEAK | | CLG SPACE PEAK | | HEATING COIL PEAK | | TEMPERATURES | | |
| Peaked at Time: Outside Air: | Mo/Hr: 7 / 15 OADB/WB/HR: 86 / 71 / 95 | Mo/Hr: Sum of OADB: 5 | Mo/Hr: Heating Design OADB: 5 | | | | | |
| Space Sens. + Lat. Btu/h | Plenum Sens. + Lat. Btu/h | Net Total Btu/h | Percent Of Total (%) | Space Sensible Btu/h | Percent Of Total (%) | Space Peak Btu/h | Coil Peak Tot Sens Btu/h | Percent Of Total (%) |
| Envelope Loads | | | | | | | | |
| SkyLite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| SkyLite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Glass Solar | 31,859 | 0 | 30 | 41,680 | 54 | -10,634 | -10,634 | 10.40 |
| Glass/Door Cond | 933 | 0 | 1 | -44 | 0 | -6,820 | -6,820 | 6.87 |
| Wall Cond | 4,271 | 0 | 4 | 4,619 | 6 | 0 | 0 | 0.00 |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Infiltration | 18,540 | 0 | 17 | 4,690 | 6 | -47,820 | -47,820 | 46.77 |
| Sub Total ==> | 55,603 | 0 | 52 | 50,944 | 66 | -65,275 | -65,275 | 63.84 |
| Internal Loads | | | | | | | | |
| Lights | 15,924 | 3,981 | 19 | 15,924 | 21 | 0 | 0 | 0.00 |
| People | 18,321 | 0 | 17 | 10,634 | 14 | 0 | 0 | 0.00 |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Sub Total ==> | 34,245 | 3,981 | 36 | 26,558 | 34 | 0 | 0 | 0.00 |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Ventilation Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Adj Air Trans Heat | 0 | 0 | 14 | 0 | 0 | 0 | -36,965 | 36.16 |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Exhaust Heat | 0 | -1,962 | -2 | 0 | 0 | 0 | 0 | 0.00 |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Duct Heat PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Underfir Sup Ht PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| Grand Total ==> | 89,848 | 2,019 | 100.00 | 77,502 | 100.00 | -65,275 | -102,240 | 100.00 |

| COOLING COIL SELECTION | | HEATING COIL SELECTION | |
|------------------------|------------------|------------------------|-----------------|
| Total Capacity ton | Sens Cap. MBH | Coil Airflow cfm | Capacity MBH |
| Main Clg | 8.9 | 106.5 | 77.4 |
| Aux Clg | 0.0 | 0.0 | 4,102 |
| Opt Vent | 0.0 | 0.0 | 61.6 |
| Total | 8.9 | 106.5 | 84.9 |

| AREAS | | HEATING COIL SELECTION | |
|--------------|--------------|------------------------|---------------------|
| Gross Total | Glass ft² | Capacity MBH | Coil Airflow cfm |
| Floor | 5,302 | -102.2 | 4,102 |
| Part | 0 | 0 | 61.6 |
| Int Door | 0 | 0 | 0 |
| EXFlr | 0 | 0 | 0 |
| Roof | 0 | 0 | 0 |
| Wall | 2,320 | 0 | 0 |
| Ext Door | 0 | 0 | 0 |
| Total | 7,622 | -102.2 | 0 |

| AIRFLOWS | | ENGINEERING CKS | |
|-------------|---------|-----------------|---------|
| Diffuser | Heating | % OA | Heating |
| Terminal | 4,102 | 13.0 | 13.0 |
| Main Fan | 4,102 | 0.77 | 0.77 |
| Sec Fan | 0 | 462.27 | 462.27 |
| Nom Vent | 533 | 597.52 | 597.52 |
| AHU Vent | 533 | 20.08 | 20.08 |
| Infil | 689 | No. People | 43 |
| Return | 4,791 | | |
| Exhaust | 1,222 | | |
| Rm Exh | 0 | | |
| Auxiliary | 0 | | |
| Leakage Dwn | 0 | | |
| Leakage Ups | 0 | | |

Project Name: MTOB 1-1-TRC
Dataset Name: MTOB 1-1-TRC

TRACE® 700 v6.2.9 calculated at 03:31 PM on 02/25/2013
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System Checksums

By ACADEMIC

Packaged Terminal Air Conditioner

AHU-04

| | COOLING COIL PEAK | | | CLG SPACE PEAK | | | HEATING COIL PEAK | | | TEMPERATURES | | | |
|----------------------|--------------------------|---------------------------|-----------------|---------------------------|----------------------|----------------------|-------------------|-------------------------------|--------------------------|----------------------|--------|---------|---------|
| | Space Sens. + Lat. Btu/h | Plenum Sens. + Lat. Btu/h | Net Total Btu/h | Mo/Hr. Sum of OADB: Peaks | Space Sensible Btu/h | Percent Of Total (%) | Space Peak Btu/h | Mo/Hr. Heating Design OADB: 5 | Coil Peak Tot Sens Btu/h | Percent Of Total (%) | SADB | Cooling | Heating |
| Envelope Loads | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56.2 | 86.7 | 70.0 |
| SkyLite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75.0 | 70.0 | 60.0 |
| SkyLite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 77.5 | 60.0 | 0.0 |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0.0 |
| Glass Solar | 36,368 | 0 | 36,368 | 45 | 42,604 | 26 | -11,835 | -11,835 | 8.80 | 0.00 | 0.0 | 0.0 | 0.0 |
| Glass/Door Cond | 1,639 | 0 | 1,639 | 1 | 1,086 | 1 | -7,590 | -7,590 | 5.65 | 0.00 | 0.0 | 0.0 | 0.0 |
| Wall Cond | 5,187 | 0 | 5,187 | 6 | 5,536 | 4 | 0 | 0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 |
| Infiltration | 26,094 | 0 | 26,094 | 10 | 9,037 | 19 | -64,488 | -64,488 | 47.97 | 0.00 | 0.0 | 0.0 | 0.0 |
| Sub Total ==> | 69,288 | 0 | 69,288 | 62 | 58,262 | 50 | -83,913 | -83,913 | 62.42 | 0.00 | 0.0 | 0.0 | 0.0 |
| Internal Loads | | | | | | | | | | | | | |
| Lights | 21,475 | 5,369 | 26,843 | 23 | 21,475 | 19 | 0 | 0 | 0.00 | 0.00 | 930 | 930 | 0 |
| People | 25,158 | 0 | 25,158 | 16 | 14,785 | 18 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 5,648 | 5,648 | 0 |
| Sub Total ==> | 46,632 | 5,369 | 52,001 | 38 | 36,260 | 37 | 0 | 0 | 0.00 | 0.00 | 1,658 | 1,658 | 0 |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Ventilation Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Adj Air Trans Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Exhaust Heat | 0 | -2,601 | -2,601 | -2 | 0 | -2 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Duct Heat PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Underfir Sup Ht PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | 0 | 0 |
| Grand Total ==> | 115,920 | 2,768 | 139,438 | 100.00 | 94,522 | 100.00 | -83,913 | -83,913 | 100.00 | 100.00 | 19,500 | 19,500 | -18,800 |

| COOLING COIL SELECTION | | | HEATING COIL SELECTION | | |
|------------------------|---------------|------------------|------------------------|------------------|------------|
| Total Capacity ton | Sens Cap. MBh | Coil Airflow cfm | Capacity MBh | Coil Airflow cfm | Lvg Ent °F |
| Main Cig | 11.6 | 139.4 | -134.4 | 4,718 | 60.0 |
| Aux Cig | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Opt Vent | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total | 11.6 | 139.4 | 0.0 | 0.0 | 0.0 |

| AREAS | | | HEATING COIL SELECTION | | |
|-------------|-----------|-----|------------------------|---------|---------|
| Gross Total | Glass ft² | (%) | Main Htg | Aux Htg | Preheat |
| Floor | 7,150 | | 0.0 | 0.0 | 0.0 |
| Part | 0 | | 0.0 | 0.0 | 0.0 |
| Int Door | 0 | | 0.0 | 0.0 | 0.0 |
| ExFir | 0 | | 0.0 | 0.0 | 0.0 |
| Roof | 0 | | 0.0 | 0.0 | 0.0 |
| Wall | 2,582 | 775 | 30 | 0.0 | 0.0 |
| Ext Door | 0 | 0 | 0 | 0.0 | 0.0 |
| Total | 0 | 0 | 0 | 0.0 | 0.0 |

| ENGINEERING CKS | | |
|-----------------|---------|---------|
| % OA | cfm/ft² | ft²/ton |
| 15.4 | 0.66 | 0.66 |
| 15.4 | 406.06 | 615.33 |
| 19.50 | 19.50 | -18.80 |
| No. People | 60 | |

Project Name: MTOB 1-1.TRC
 Dataset Name: MTOB 1-1.TRC

TRACE® 700 v6.2.9 calculated at 03:31 PM on 02/25/2013
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E.4 TRACE room checksums

Room Checksums By ACADEMIC

220 Office

| Peaked at Time: Outside Air: | COOLING COIL PEAK | | | CLG SPACE PEAK | | | HEATING COIL PEAK | | | TEMPERATURES | | | | | | |
|---------------------------------|---|---------------------------|----------------------------------|-----------------------|---------------------------------|-----------------------|----------------------------|----------------------------|----------------------------|----------------|---------------------|--------------------|----------------------------|------|---------|---------|
| | Mo/Hr: 7 / 17 OADB/WB/HR: 84 / 69 / 90 | Mo/Hr: 6 / 17 OADB: 82 | Mo/Hr: Heating Design OADB: 5 | Sens. + Lat. Btu/h | Plenum Sens. + Lat. Btu/h | Net Total Btu/h | Percent Of Total (%) | Space Sensible Btu/h | Percent Of Total (%) | Envelope Loads | Space Sens Btu/h | Coil Sens Btu/h | Percent Of Total (%) | SADB | Cooling | Heating |
| Envelope Loads | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 58.4 | 87.1 | |
| Skylite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75.0 | 70.0 | |
| Skylite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75.5 | 65.3 | |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 76.2 | 0.0 | |
| Glass Solar | 2,835 | 0 | 2,835 | 45 | 0 | 2,835 | 61 | 3,029 | 0 | -1,787 | -1,787 | 27.44 | 0 | 0.0 | 0.0 | |
| Glass/Door Cond | 262 | 0 | 262 | 4 | 0 | 262 | 10 | 197 | 0 | -1,146 | -1,146 | 17.60 | 0 | 0.0 | 0.0 | |
| Wall Cond | 522 | 0 | 522 | 8 | 0 | 522 | 10 | 502 | 0 | 0 | 0 | 0.00 | 0 | 0.0 | 0.0 | |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.0 | 0.0 | |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.0 | 0.0 | |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.0 | 0.0 | |
| Infiltration | 756 | 0 | 756 | 12 | 0 | 756 | 4 | 216 | 0 | -2,165 | -2,165 | 33.23 | 0 | 0.0 | 0.0 | |
| Sub Total ==> | 4,374 | 0 | 4,374 | 70 | 0 | 4,374 | 79 | 3,945 | 0 | -5,098 | -5,098 | 78.27 | 0 | 0.0 | 0.0 | |
| Internal Loads | | | | | | | | | | | | | | | | |
| Lights | 721 | 180 | 901 | 14 | 0 | 901 | 15 | 721 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| People | 540 | 0 | 540 | 9 | 0 | 540 | 6 | 300 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Sub Total ==> | 1,261 | 180 | 1,441 | 23 | 0 | 1,441 | 21 | 1,021 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Ventilation Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Adj Air Trans Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Exhaust Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Duct Heat PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Underfir Sup Ht PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0.00 | 0.00 | |
| Grand Total ==> | 5,635 | 150 | 6,280 | 100.00 | 0 | 6,280 | 100.00 | 4,965 | 0 | -5,098 | -5,098 | 100.00 | 0 | 0.00 | 0.00 | |

| COOLING COIL SELECTION | | | HEATING COIL SELECTION | | | | | | |
|------------------------|------------------|---------------------|------------------------|-------------|-------------|-----------------|---------------------|-------------|-------------|
| Total Capacity ton | Sens Cap. MBh | Coil Airflow cfm | Enter °F | Leave °F | gr/lb | Capacity MBh | Coil Airflow cfm | Ent °F | Lvg °F |
| 0.5 | 6.3 | 280 | 76.2 | 63.1 | 69.4 | 58.4 | 55.5 | 64.3 | 64.3 |
| 0.0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.0 | 0.0 | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.5 | 6.3 | 280 | 76.2 | 63.1 | 69.4 | 58.4 | 55.5 | 64.3 | 64.3 |
| Total | 0.5 | 6.3 | 280 | 76.2 | 63.1 | 69.4 | 58.4 | 55.5 | 64.3 |

| AREAS | | |
|--------------|--------------|-------------------|
| Gross Total | Glass ft² | Percentage (%) |
| 240 | 0 | 0 |
| Floor | 0 | 0 |
| Part | 0 | 0 |
| Int Door | 0 | 0 |
| Ext Door | 0 | 0 |
| Roof | 0 | 0 |
| Wall | 390 | 117 |
| Ext Door | 0 | 0 |
| Total | 390 | 117 |

| ENGINEERING CKS | | |
|-----------------|---------|------------|
| Cooling | Heating | No. People |
| 7.3 | 7.3 | 1 |
| 1.17 | 1.17 | |
| 534.78 | | |
| 458.62 | | |
| 26.17 | -27.14 | |

Project Name: MTOB 1-1.TRC
Dataset Name: MTOB 1-1.TRC

TRACE® 700 v6.2.9 calculated at 03:31 PM on 02/25/2013
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Room Checksums By ACADEMIC

306 Office

| | COOLING COIL PEAK | | | | CLG SPACE PEAK | | | | HEATING COIL PEAK | | | | TEMPERATURES | | | |
|---------------------------|--------------------------|---------------------|--------------|------------------|----------------|------------------|-----------------------|------------------|-------------------|---------------|------------------|--------|--------------|---------|--|--|
| | Space Sens. + Lat. | Plenum Sens. + Lat. | Net Total | Percent Of Total | Space Sensible | Percent Of Total | Envelope Loads | Percent Of Total | Space Peak | Coil Peak | Percent Of Total | SADB | Cooling | Heating | | |
| Mo/Hr: Outside Air: | Mo/Hr: 7 / 8 | | | Mo/Hr: 7 / 8 | | | Mo/Hr: Heating Design | | | | | | | | | |
| | OADB/WBtHR: 69 / 65 / 88 | | | OADB: 69 | | | OADB: 5 | | | | | | | | | |
| Envelope Loads | | | | | | | | | | | | | | | | |
| SkyLite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56.9 | 87.9 | | |
| SkyLite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75.0 | 70.0 | | |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75.7 | 70.0 | | |
| Glass Solar | 1,906 | 0 | 1,906 | 62 | 1,906 | 77 | 1,906 | 62 | 1,906 | 77 | 0 | 0 | 75.0 | 63.6 | | |
| Glass/Door Cond | -88 | 0 | -88 | -2 | -88 | -3 | -88 | -2 | -88 | -3 | -673 | -673 | 0.0 | 0.0 | | |
| Wall Cond | 131 | 0 | 131 | 4 | 131 | 5 | 131 | 4 | 131 | 5 | -432 | -432 | 0.0 | 0.0 | | |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | | |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | | |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | | |
| Infiltration | 140 | 0 | 140 | 5 | -127 | -5 | 140 | 5 | -1,353 | -40.48 | -1,353 | -1,353 | 0.0 | 0.0 | | |
| Sub Total ==> | 2,109 | 0 | 2,109 | 69 | 1,842 | 74 | 2,109 | 69 | -2,458 | -73.53 | -2,458 | -2,458 | 0.0 | 0.0 | | |
| Internal Loads | | | | | | | | | | | | | | | | |
| Lights | 451 | 113 | 563 | 18 | 451 | 18 | 563 | 18 | 0 | 0 | 0 | 0 | 20 | 20 | | |
| People | 338 | 0 | 338 | 11 | 188 | 8 | 338 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 148 | 148 | | |
| Sub Total ==> | 788 | 113 | 901 | 29 | 638 | 26 | 901 | 29 | 0 | 0 | 0 | 0 | 32 | 32 | | |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ventilation Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Adj Air Trans Heat | 0 | 0 | 91 | 3 | 0 | 0 | 91 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Exhaust Heat | 0 | -25 | -25 | -1 | 0 | 0 | -25 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Duct Heat PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Underfir Sup Ht PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Grand Total ==> | 2,897 | 88 | 3,077 | 100.00 | 2,480 | 100.00 | 3,077 | 100.00 | -2,458 | -3,342 | 100.00 | | | | | |

| AIRFLOWS | | AIRFLOWS | |
|-------------|---------|----------|---------|
| | Cooling | Heating | Heating |
| Diffuser | 129 | 129 | 129 |
| Terminal | 129 | 129 | 129 |
| Main Fan | 129 | 129 | 129 |
| Sec Fan | 0 | 0 | 0 |
| Nom Vent | 13 | 13 | 13 |
| AHU Vent | 13 | 13 | 13 |
| Infil | 20 | 20 | 20 |
| MinStop/Rh | 0 | 0 | 0 |
| Return | 148 | 148 | 148 |
| Exhaust | 32 | 32 | 32 |
| Rm Exh | 0 | 0 | 0 |
| Auxiliary | 0 | 0 | 0 |
| Leakage Dwn | 0 | 0 | 0 |
| Leakage Ups | 0 | 0 | 0 |

| ENGINEERING CKS | | |
|-----------------|-----------------|--------|
| | Cooling Heating | |
| % OA | 9.9 | 9.9 |
| cfm/ft² | 0.86 | 0.86 |
| cfm/ton | 501.84 | |
| ft³/ton | 585.04 | |
| Btu/hr-ft² | 20.51 | -22.28 |
| No. People | 1 | |

| HEATING COIL SELECTION | | HEATING COIL SELECTION | |
|------------------------|-------------|------------------------|---------|
| | Capacity | Coil Airflow | Ent Lvg |
| | MBh | cfm | °F |
| Main Htg | -3.3 | 129 | 63.6 |
| Aux Htg | 0.0 | 0 | 0.0 |
| Preheat | 0.0 | 0 | 0.0 |
| Humidif | 0.0 | 0 | 0.0 |
| Opt Vent | 0.0 | 0 | 0.0 |
| Total | -3.3 | | |

| AREAS | | AREAS | |
|--------------|-------------|-------|---------|
| | Gross Total | Glass | ft² (%) |
| Floor | 150 | | |
| Part | 0 | | |
| Int Door | 0 | | |
| ExPr | 0 | | |
| Roof | 0 | | |
| Wall | 147 | 44 | 30 |
| Ext Door | 0 | 0 | 0 |
| Total | | | |

| COOLING COIL SELECTION | | COOLING COIL SELECTION | |
|------------------------|------------|------------------------|----------------|
| | Sens Cap. | Coil Airflow | Enter DB/WBtHR |
| | ton | cfm | °F |
| Main Clg | 0.3 | 129 | 75.0 |
| Aux Clg | 0.0 | 0 | 0.0 |
| Opt Vent | 0.0 | 0 | 0.0 |
| Total | 0.3 | | |

| COOLING COIL SELECTION | | COOLING COIL SELECTION | |
|------------------------|------------|------------------------|----------------|
| | Sens Cap. | Coil Airflow | Enter DB/WBtHR |
| | ton | cfm | °F |
| Main Clg | 0.3 | 129 | 75.0 |
| Aux Clg | 0.0 | 0 | 0.0 |
| Opt Vent | 0.0 | 0 | 0.0 |
| Total | 0.3 | | |

Project Name: MTOB 1-1.TRC
Dataset Name: MTOB 1-1.TRC

TRACE® 700 v6.2.9 calculated at 03:31 PM on 02/25/2013
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Room Checksums

By ACADEMIC

309 Office

| | COOLING COIL PEAK | | | CLG SPACE PEAK | | | HEATING COIL PEAK | | | TEMPERATURES | | |
|---------------------------|--------------------------------|---------------------------------|-----------------------|----------------------------|----------------------------|----------------------------|---------------------|--------------------------------|----------------------------|---------------|---------------|---------|
| | Space Sens. + Lat. Btu/h | Plenum Sens. + Lat. Btu/h | Net Total Btu/h | Space Sensible Btu/h | Percent Of Total (%) | Percent Of Total (%) | Space Peak Btu/h | Coil Peak Tot Sens Btu/h | Percent Of Total (%) | SADB | Cooling | Heating |
| Envelope Loads | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 39.8 | 125.0 | |
| Skylite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 75.0 | 70.0 | |
| Skylite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 77.5 | 34.0 | |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 82.2 | 0.0 | |
| Glass Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | |
| Glass/Door Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | |
| Wall Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0.0 | 0.0 | |
| Infiltration | 575 | 0 | 575 | 229 | 26 | 33 | -1,353 | -1,353 | 60.47 | 0.0 | 0.0 | |
| Sub Total ==> | 575 | 0 | 575 | 229 | 26 | 33 | -1,353 | -1,353 | 60.47 | 0.0 | 0.0 | |
| Internal Loads | | | | | | | | | | | | |
| Lights | 451 | 113 | 563 | 451 | 52 | 32 | 0 | 0 | 0.00 | 0 | 0 | |
| People | 338 | 0 | 338 | 188 | 22 | 19 | 0 | 0 | 0.00 | 0 | 0 | |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Sub Total ==> | 788 | 113 | 901 | 638 | 74 | 51 | 0 | 0 | 0.00 | 0 | 0 | |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Ventilation Load | 0 | 0 | 376 | 0 | 0 | 21 | 0 | -885 | 39.53 | 0 | 0 | |
| Adj Air Trans Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Exhaust Heat | 0 | -85 | -85 | 0 | 0 | -5 | 0 | 0 | 0.00 | 0 | 0 | |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Duct Heat PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Underfir Sup Ht PkUp | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 | 0 | 0 | |
| Grand Total ==> | 1,363 | 27 | 1,766 | 867 | 100.00 | 100.00 | -1,353 | -2,237 | 100.00 | 11,777 | -14.92 | |

| COOLING COIL SELECTION | | HEATING COIL SELECTION | |
|------------------------|------------------|------------------------|-------------|
| Total Capacity ton | Sens Cap. MBh | Coil Airflow cfm | Enter °F |
| 0.2 | 1.8 | 23 | 82.2 |
| 0.0 | 0.0 | 0 | 0.0 |
| 0.0 | 0.0 | 0 | 0.0 |
| 0.2 | 1.8 | 0 | 0.0 |
| Total | 0.2 | 23 | 82.2 |

| AREAS | | HEATING COIL SELECTION | |
|--------------|--------------|------------------------|---------------------|
| Gross Total | Glass ft² | Capacity MBh | Coil Airflow cfm |
| 150 | 0 | -2.2 | 23 |
| Floor | 0 | 0.0 | 34.0 |
| Part | 0 | 0.0 | 0.0 |
| Int Door | 0 | -0.1 | 0.0 |
| ExPr | 0 | 0.0 | 39.8 |
| Roof | 0 | 0.0 | 0.0 |
| Wall | 0 | 0.0 | 0.0 |
| Ext Door | 0 | -2.2 | 0.0 |
| Total | 150 | -2.2 | 125.0 |

| ENGINEERING CKS | |
|-----------------|------------|
| | No. People |
| % OA | 1 |
| cmfrft² | 11.77 |
| cfm/ton | 156.64 |
| ft³/ton | 1,019.50 |
| Btu/hr-ft² | -14.92 |

Project Name: MTOB 1-1,TRC
Dataset Name:

TRACE® 700 v6.2.9 calculated at 03:31 PM on 02/25/2013
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Room Checksums By ACADEMIC

320 Conference

| | COOLING COIL PEAK | | | | CLG SPACE PEAK | | | | HEATING COIL PEAK | | | | TEMPERATURES | | | | | | |
|----------------------|--------------------------------|---------------------------------|-----------------------|----------------------------|----------------------------|-------------------------------------|----------------------|---------------------|--------------------------------|----------------------------|------|---------|--------------|-----------|--------|-------|----------|----------|----------|
| | Space Sens. + Lat. Btu/h | Plenum Sens. + Lat. Btu/h | Net Total Btu/h | Percent Of Total (%) | Space Sensible Btu/h | Space Percent Of Total (%) | Envelope Loads | Space Peak Btu/h | Coil Peak Tot Sens Btu/h | Percent Of Total (%) | SADB | Cooling | Heating | Ra Plenum | Return | RetoA | Fn MtrTD | Fn BidTD | Fn Frict |
| Envelope Loads | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sky/ite Solar | 0 | 0 | 0 | 0 | 0 | 0 | Sky/ite Solar | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sky/ite Cond | 0 | 0 | 0 | 0 | 0 | 0 | Sky/ite Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | Roof Cond | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Glass Solar | 1,007 | 0 | 1,007 | 6 | 4,639 | 42 | Glass Solar | -1,638 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Glass/Door Cond | 289 | 0 | 289 | 2 | -165 | -2 | Glass/Door Cond | -1,051 | -1,638 | 10.36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Wall Cond | 302 | 0 | 302 | 2 | 319 | 6.64 | Wall Cond | -1,051 | -1,051 | 6.64 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | Partition/Door | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Floor | 0 | 0 | 0 | 0 | 0 | 0 | Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | Adjacent Floor | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Infiltration | 1,684 | 0 | 1,684 | 10 | -364 | -3 | Infiltration | -3,878 | -3,878 | 24.52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sub Total ==> | 3,261 | 0 | 3,261 | 19 | 4,429 | 40 | Sub Total ==> | -6,567 | -6,567 | 41.52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Internal Loads | | | | | | | Internal Loads | | | | | | | | | | | | |
| Lights | 1,291 | 323 | 1,614 | 9 | 1,291 | 12 | Lights | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| People | 8,600 | 0 | 8,600 | 50 | 5,268 | 48 | People | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Misc | 0 | 0 | 0 | 0 | 0 | 0 | Misc | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sub Total ==> | 9,891 | 323 | 10,214 | 59 | 6,559 | 60 | Sub Total ==> | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | Ceiling Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ventilation Load | 0 | 0 | 0 | 0 | 0 | 0 | Ventilation Load | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj Air Trans Heat | 0 | 0 | 4,015 | 23 | 0 | 0 | Adj Air Trans Heat | -9,248 | -9,248 | 58.48 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Dehumid. Ov Sizing | 0 | 0 | 0 | 0 | 0 | 0 | Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ov/Undr Sizing | 0 | 0 | 0 | 0 | 0 | 0 | Exhaust Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exhaust Heat | 0 | -126 | -126 | -1 | 0 | 0 | OA Preheat Diff. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sup. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | RA Preheat Diff. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ret. Fan Heat | 0 | 0 | 0 | 0 | 0 | 0 | Additional Reheat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Duct Heat Pkup | 0 | 0 | 0 | 0 | 0 | 0 | System Plenum Heat | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Underfir Sup Ht Pkup | 0 | 0 | 0 | 0 | 0 | 0 | Underfir Sup Ht Pkup | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | Supply Air Leakage | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total ==> | 13,152 | 197 | 17,364 | 100.00 | 10,988 | 100.00 | Grand Total ==> | -6,567 | -15,816 | 100.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| AIRFLOWS | |
|-------------|-----|
| Diffuser | 428 |
| Terminal | 428 |
| Main Fan | 428 |
| Sec Fan | 0 |
| Nom Vent | 133 |
| AHU Vent | 133 |
| Infil | 56 |
| MinStop/Rh | 0 |
| Return | 484 |
| Exhaust | 189 |
| Rm Exh | 0 |
| Auxiliary | 0 |
| Leakage Dwn | 0 |
| Leakage Ups | 0 |

| ENGINEERING CKS | |
|-----------------|--------|
| % OA | 31.1 |
| cfm/ft² | 1.00 |
| cfm/ton | 295.89 |
| ft³/ton | 297.17 |
| Btu/hr-ft² | 40.38 |
| No. People | 22 |

| HEATING COIL SELECTION | | | |
|------------------------|--------------|-----|------|
| Capacity | Coil Airflow | Ent | Lvg |
| MBh | cfm | °F | °F |
| Main Htg | -15.8 | 428 | 49.8 |
| Aux Htg | 0.0 | 0.0 | 0.0 |
| Preheat | -0.6 | 428 | 49.8 |
| Humidif | 0.0 | 0 | 0.0 |
| Opt Vent | 0.0 | 0 | 0.0 |
| Total | -15.8 | | |

| AREAS | | |
|--------------|------------|-----------|
| Gross Total | Glass | (%) |
| ft² | ft² | |
| Floor | 430 | |
| Part | 0 | |
| Int Door | 0 | |
| ExPr | 0 | |
| Roof | 0 | |
| Wall | 358 | 107 |
| Ext Door | 0 | 0 |
| Total | 788 | 30 |

| COOLING COIL SELECTION | | |
|------------------------|------------|--------------|
| Total Capacity | Sens Cap. | Coil Airflow |
| ton | MBh | cfm |
| Main Cig | 1.5 | 17.4 |
| Aux Cig | 0.0 | 0.0 |
| Opt Vent | 0.0 | 0.0 |
| Total | 1.5 | 17.4 |

| COOLING COIL SELECTION | | | |
|------------------------|---------|-------|---------|
| Enter | DBWB/HR | Leave | DBWB/HR |
| °F | gr/lb | °F | gr/lb |
| 51.0 | 50.9 | 57.8 | |
| 0.0 | 0.0 | 0.0 | |
| 0.0 | 0.0 | 0.0 | |
| 0.0 | 0.0 | 0.0 | |

Project Name: MTOB 1-1.TRC
Dataset Name: MTOB 1-1.TRC

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E.5 IBC tables used

SECTION 503 GENERAL BUILDING HEIGHT AND AREA LIMITATIONS

TABLE 503
ALLOWABLE BUILDING HEIGHTS AND AREAS^a
Building height limitations shown in feet above grade plane. Story limitations shown as stories above grade plane.
Building area limitations shown in square feet, as determined by the definition of "Area, building," per story

| GROUP | HEIGHT (feet) | TYPE OF CONSTRUCTION | | | | | | | |
|-------|---------------|------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | | TYPE I | | TYPE II | | TYPE III | | TYPE IV | T |
| | | A | B | A | B | A | B | HT | A |
| | UL | 160 | 65 | 55 | 65 | 55 | 65 | 50 | |
| | | STORIES(S) AREA (A) | | | | | | | |
| A-1 | S A | UL UL | 5 UL | 3 15,500 | 2 8,500 | 3 14,000 | 2 8,500 | 3 15,000 | 2 11,500 |
| A-2 | S A | UL UL | 11 UL | 3 15,500 | 2 9,500 | 3 14,000 | 2 9,500 | 3 15,000 | 2 11,500 |
| A-3 | S A | UL UL | 11 UL | 3 15,500 | 2 9,500 | 3 14,000 | 2 9,500 | 3 15,000 | 2 11,500 |
| A-4 | S A | UL UL | 11 UL | 3 15,500 | 2 9,500 | 3 14,000 | 2 9,500 | 3 15,000 | 2 11,500 |
| A-5 | S A | UL UL | UL UL | UL UL | UL UL | UL UL | UL UL | UL UL | UL UL |
| B | S A | UL UL | 11 UL | 5 37,500 | 3 23,000 | 5 28,500 | 3 19,000 | 5 36,000 | 3 18,000 |
| E | S A | UL UL | 5 UL | 3 26,500 | 2 14,500 | 3 23,500 | 2 14,500 | 3 25,500 | 1 18,500 |
| F-1 | S A | UL UL | 11 UL | 4 25,000 | 2 15,500 | 3 19,000 | 2 12,000 | 4 33,500 | 2 14,000 |
| F-2 | S A | UL UL | 11 UL | 5 37,500 | 3 23,000 | 4 28,500 | 3 18,000 | 5 50,500 | 3 21,000 |
| H-1 | S A | 1 21,000 | 1 16,500 | 1 11,000 | 1 7,000 | 1 9,500 | 1 7,000 | 1 10,500 | 1 7,500 |



**TABLE 601
FIRE-RESISTANCE RATING REQUIREMENTS FOR BUILDING ELEMENTS (hours)**

| BUILDING ELEMENT | TYPE I | | TYPE II | | TYPE III | | TYPE IV | TYPE V | |
|--|-------------------------------|------------------|------------------|----------------|------------------|---|---------------------|------------------|---|
| | A | B | A ^d | B | A ^d | B | HT | A ^d | B |
| Primary structural frame ^g (see Section 202) | 3 ^a | 2 ^a | 1 | 0 | 1 | 0 | HT | 1 | 0 |
| Bearing walls | | | | | | | | | |
| Exterior ^{f, g} | 3 | 2 | 1 | 0 | 2 | 2 | 2 | 1 | 0 |
| Interior | 3 ^a | 2 ^a | 1 | 0 | 1 | 0 | 1/HT | 1 | 0 |
| Nonbearing walls and partitions | See Table 602 | | | | | | | | |
| Exterior | | | | | | | | | |
| Nonbearing walls and partitions | | | | | | | See Section 602.4.6 | | |
| Interior ^e | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Floor construction and secondary members (see Section 202) | 2 | 2 | 1 | 0 | 1 | 0 | HT | 1 | 0 |
| Roof construction and secondary members (see Section 202) | 1 ^{1/2} ^b | 1 ^{b,c} | 1 ^{b,c} | 0 ^c | 1 ^{b,c} | 0 | HT | 1 ^{b,c} | 0 |

For SI: 1 foot = 304.8 mm.

- a. Roof supports: Fire-resistance ratings of primary structural frame and bearing walls are permitted to be reduced by 1 hour where supporting a roof only.
- b. Except in Group F-1, H, M and S-1 occupancies, fire protection of structural members shall not be required, including protection of roof framing and decking where every part of the roof construction is 20 feet or more above any floor immediately below. Fire-retardant-treated wood members shall be allowed to be used for such unprotected members.
- c. In all occupancies, heavy timber shall be allowed where a 1-hour or less fire-resistance rating is required.
- d. An approved automatic sprinkler system in accordance with Section 903.3.1.1 shall be allowed to be substituted for 1-hour fire-resistance-rated construction, provided such system is not otherwise required by other provisions of the code or used for an allowable area increase in accordance with Section 506.3 or an allowable height increase in accordance with Section 504.2. The 1-hour substitution for the fire resistance of exterior walls shall not be permitted.
- e. Not less than the fire-resistance rating required by other sections of this code.
- f. Not less than the fire-resistance rating based on fire separation distance (see Table 602).
- g. Not less than the fire-resistance rating as referenced in Section 704.10

appendix F: additional drawings

